

EXHIBIT A

LEGAL DESCRIPTION

Real property in the City of , County of Riverside, State of California, described as follows:

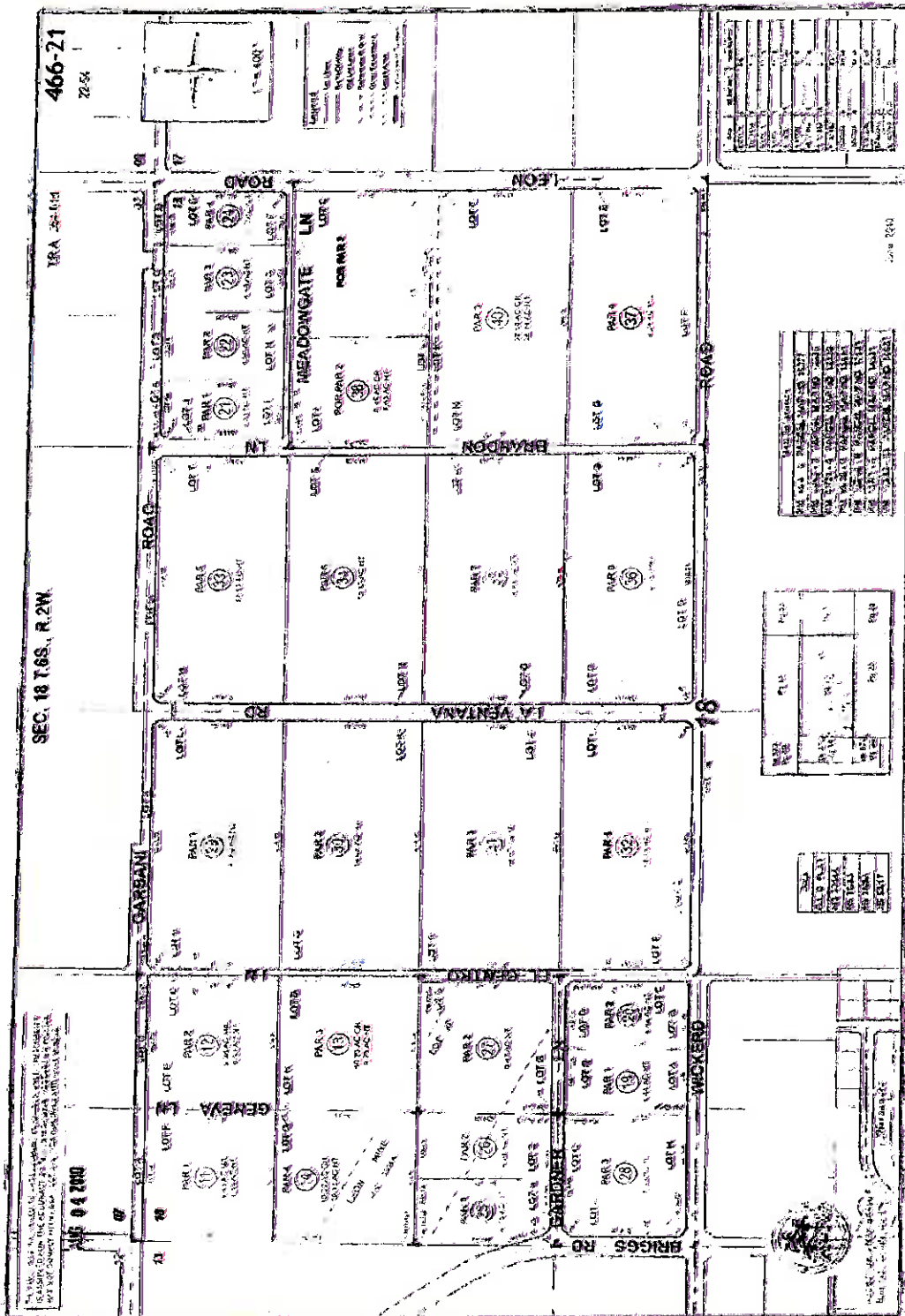
PARCEL 1: (APN: 466-210-029, 466-210-030, 466-210-031, 466-210-032, 466-210-033, 466-210-034, 466-210-035 AND 466-210-036)

PARCELS 1 THROUGH 8, INCLUSIVE, AND LETTERED LOTS "A" THROUGH "T", INCLUSIVE OF PARCEL MAP NO. 18607, IN THE COUNTY OF RIVERSIDE, STATE OF CALIFORNIA, AS PER MAP RECORDED IN BOOK 113 PAGES 52 AND 53 OF PARCEL MAPS, IN THE OFFICE OF THE COUNTY RECORDER OF SAID COUNTY.

PARCEL 2: (APN: 466-210-038)

PARCEL B OF LOT LINE ADJUSTMENT NO. 5355 RECORDED JANUARY 11, 2010 AS INSTRUMENT NO. 2010-0010216 OF OFFICIAL RECORDS, DESCRIBED AS FOLLOWS:

THOSE PORTIONS OF PARCEL 2 AND LOT "L" OF PARCEL MAP NO. 10277, IN THE COUNTY OF RIVERSIDE, STATE OF CALIFORNIA, AS PER MAP RECORDED IN BOOK 46, PAGE 8 OF PARCEL MAPS, IN THE OFFICE OF THE COUNTY RECORDER OF SAID COUNTY, LYING WEST OF A LINE THAT IS PARALLEL WITH AND DISTANT 527.39 FEET, AS MEASURED AT RIGHT ANGLES TO THE WEST LINE OF SAID PARCEL 2.



466-21
22-54

SEC. 18 T.6S. R.2W.

466-04200

THIS PLAT WAS PREPARED BY THE FIRST AMERICAN TITLE INSURANCE COMPANY, CHICAGO, ILL. ON THE 28th DAY OF JANUARY 1928. THE ORIGINAL RECORD OF THIS PLAT IS IN THE OFFICE OF THE COUNTY CLERK OF COOK COUNTY, ILL. AT CHICAGO, ILL. A TRUE AND CORRECT COPY OF THIS PLAT IS ON FILE IN THE OFFICE OF THE COUNTY CLERK OF COOK COUNTY, ILL. AT CHICAGO, ILL.



Legend
 As Shown
 By Reference
 To Other
 Plats
 In This
 Record
 As Shown
 In This
 Record
 As Shown
 In This
 Record

Lot No.	Acres	Owner
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Lot No.	Acres	Owner
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Dawson, Brett

From: Joe Castaneda <joe@jlcengineering.com>
Sent: Tuesday, June 14, 2016 11:34 AM
To: Jilleen Ferris
Subject: Fwd: La Ventana - Final Revision to COA
Attachments: image001.gif

Joe Castaneda
Principal
JLC Engineering & Consulting
951.304-9552
Sent from I-Phone

Begin forwarded message:

From: "Larry R. Markham" <lrmarkham@markhamdmg.com>
Date: June 10, 2016 at 5:16:14 PM PDT
To: Joseph Rivani <JRivani@GIDLLCO.COM>, "Alhadeff, Samuel" <Samuel.Alhadeff@lewisbrisbois.com>, Joe Castaneda <joe@jlcengineering.com>
Subject: RE: La Ventana - Final Revision to COA

THX

From: Joseph Rivani [mailto:JRivani@GIDLLCO.COM]
Sent: Friday, June 10, 2016 5:01 PM
To: Alhadeff, Samuel; Joe Castaneda; Larry R. Markham
Subject: RE: La Ventana - Final Revision to COA

Consider it approved.

Respectfully,

Joseph Rivani

Global Investment & Development, LLC

3470 Wilshire Blvd, Suite 1020
Los Angeles, CA 90010
Tel: 213.365.0005
Cell: 213.369.9600
Fax: 213.365.0405

From: Alhadeff, Samuel [mailto:Samuel.Alhadeff@lewisbrisbois.com]
Sent: Friday, June 10, 2016 10:15 AM
To: 'Joe Castaneda' <joe@jlcengineering.com>; Larry R. Markham <lrmarkham@markhamdmg.com>
Cc: Joseph Rivani <JRivani@GIDLLCO.COM>
Subject: RE: La Ventana - Final Revision to COA

:: 951.304.3568 – Fax

JLC Engineering & Consulting Inc.
36263 Calle de Lobo
Murrieta, CA 92562



May 24, 2016

Joseph Rivani

Global Investment & Development, LLC

3470 Wilshire Blvd., Suite 1020

Los Angeles, CA 90010

Subject: Drainage Acceptance by KGK Riverside Properties, LLC
TM 36785/APN 466-210-029 to 036 & 038

Dear Mr. Rivani,

The civil engineer retained by KGK, Larry Markham, MDMG, Inc. has reviewed the following documents provided by Joe Castaneda, JLC Engineering & Consulting Inc., submitted on behalf of Tentative Tract Map 36785 prepared for the applicant Joseph Rivani, Global Investment & Development, LLC.

1. Pre Project Condition

Site Hydrology Map

Exhibit A, TM 36785

2. Post Project Condition

Offsite Hydrology Map

Exhibit B-1, TM 36785

3. Post Project Condition

Onsite Hydrology Map

Exhibit B-2, TM 36785

4. Post Project Flow Rate Exhibit

5. Rational Hydrology Studies – TM 36785 All 100 year Storm Event Hydrology Calculations

- a. Post Project – Onsite Area A
- b. Post Project – Onsite Area B
- c. Post Project – Onsite Area C
- d. Post Project – Onsite Area D
- e. Post Project – Onsite Area E
- f. Pre Project – Onsite Area F
- g. Post Project – Offsite Area F
- h. Post Project – Onsite Area Q
- i. Post Project – Onsite Area T

6. Line 1 Storm Drain Outlet

Proposed Access and Easement

Figure A-1 – Alternative #1

7. JLC email dated 4/6/16, 6:13am to Larry Markham, copied to J. Rivani.

The civil engineer for KGK finds the preliminary exhibits and hydrology calculations acceptable for the purpose of tentative tract approval and to be subject to the review and approval of the final hydrology and hydraulic calculations to be approved to the Riverside County Transportation Department (RCTD) and Riverside County Flood Control and Water Conservation District (RCFCWCD) and the civil engineer for KGK.

The civil engineer for KGK finds that Alternative #1 of the JLC email of 4/6/16, 6:13am acceptable as depicted. Alternative #2 depicted in the same JLC email is not acceptable. This acceptance is for the preliminary design of the Line 1 Storm Drain and is to be subject to final approval of the Line 1 Storm Drain improvement plans by RCTD and RCFCWCD and the civil engineer for KGK.

The Alternative #1 design shall be accepted for maintenance by RCFCWCD upon completion of construction.

KGK shall dedicate the south half width right of way for Wickerd Road to the County of Riverside to provide for the construction of the Line 1 Storm Drain. The dedication documents shall be prepared by Rivani, JVRL 220 or their successors in interest at no cost to KGK. KGK shall also provide for RCFCWCD maintenance access easements needed to maintain the Line 1 Storm Drain.

The dedication and easements shall be provided upon approval of the hydrology and hydraulic calculations and improvement plans for the Line 1 Storm Drain, by RCTD and RCFCWCD and the civil engineer for KGK.

This drainage acceptance shall be reflected within the Conditions of Approval for TM 36785 and/or any my subsequent or superseding approvals for this subject drainage area.

Rivani, JVRL 220 LLC or their successors in interest shall endorse and support any land use application proposed by KGK or their successors in interest that is similar in nature to the TM 36785.

This drainage acceptance shall be memorialized by means of a covenant recorded on the Rivani JVRL 220 LLC property, recorded in favor of KGK recorded prior to approval by Board of Supervisors.

Cc: Russell Williams, RCTD

Henry Olivo, RCFCWCD

Attachments: Items 1. through 7.

William Feunmann
for KGK

6/16/16

Item 1

TENTATIVE TRACT MAP 36785 COUNTY OF RIVERSIDE, STATE OF CALIFORNIA PRE-PROJECT CONDITION SITE HYDROLOGY MAP

SHEET 1 OF 1

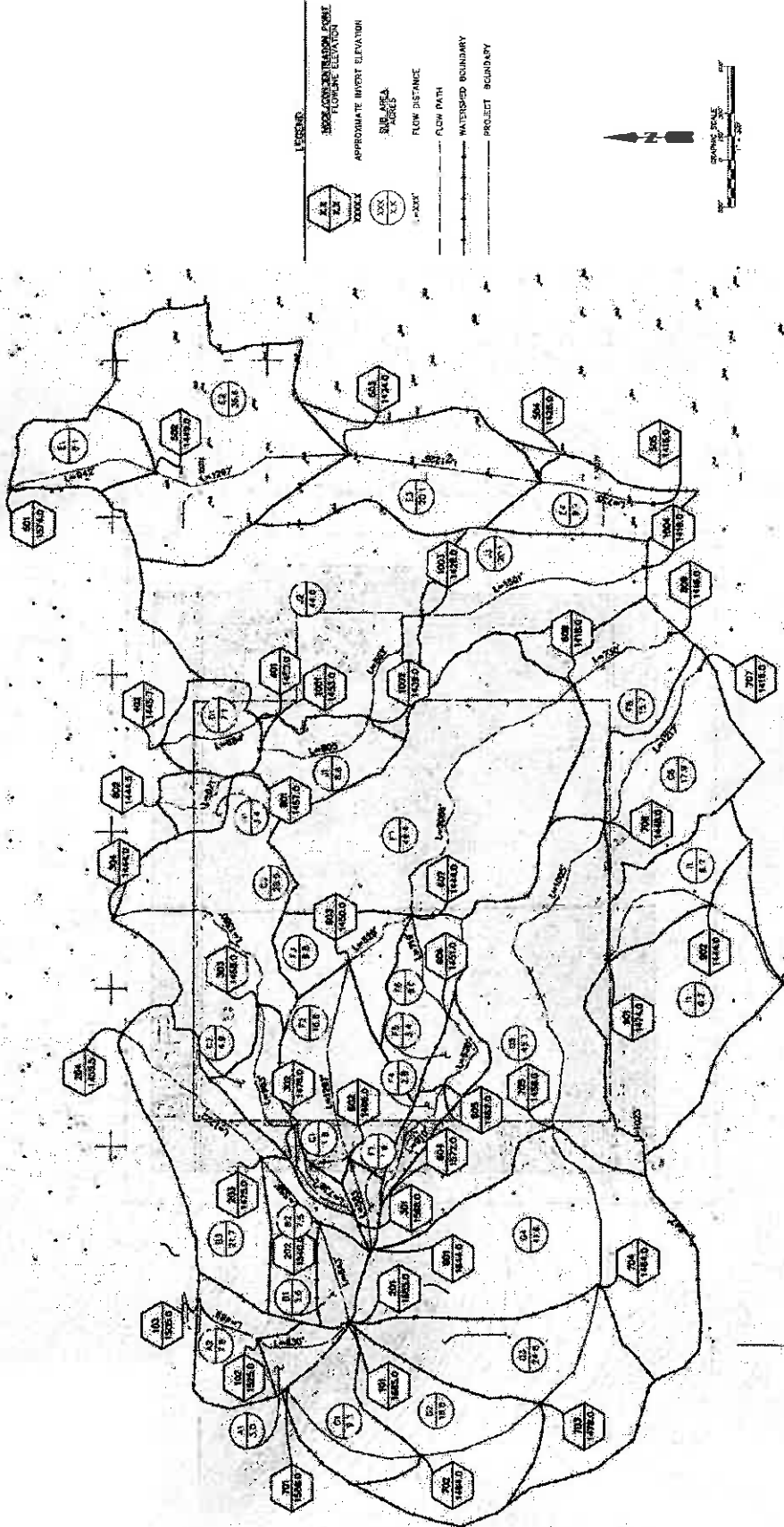


EXHIBIT 'A'

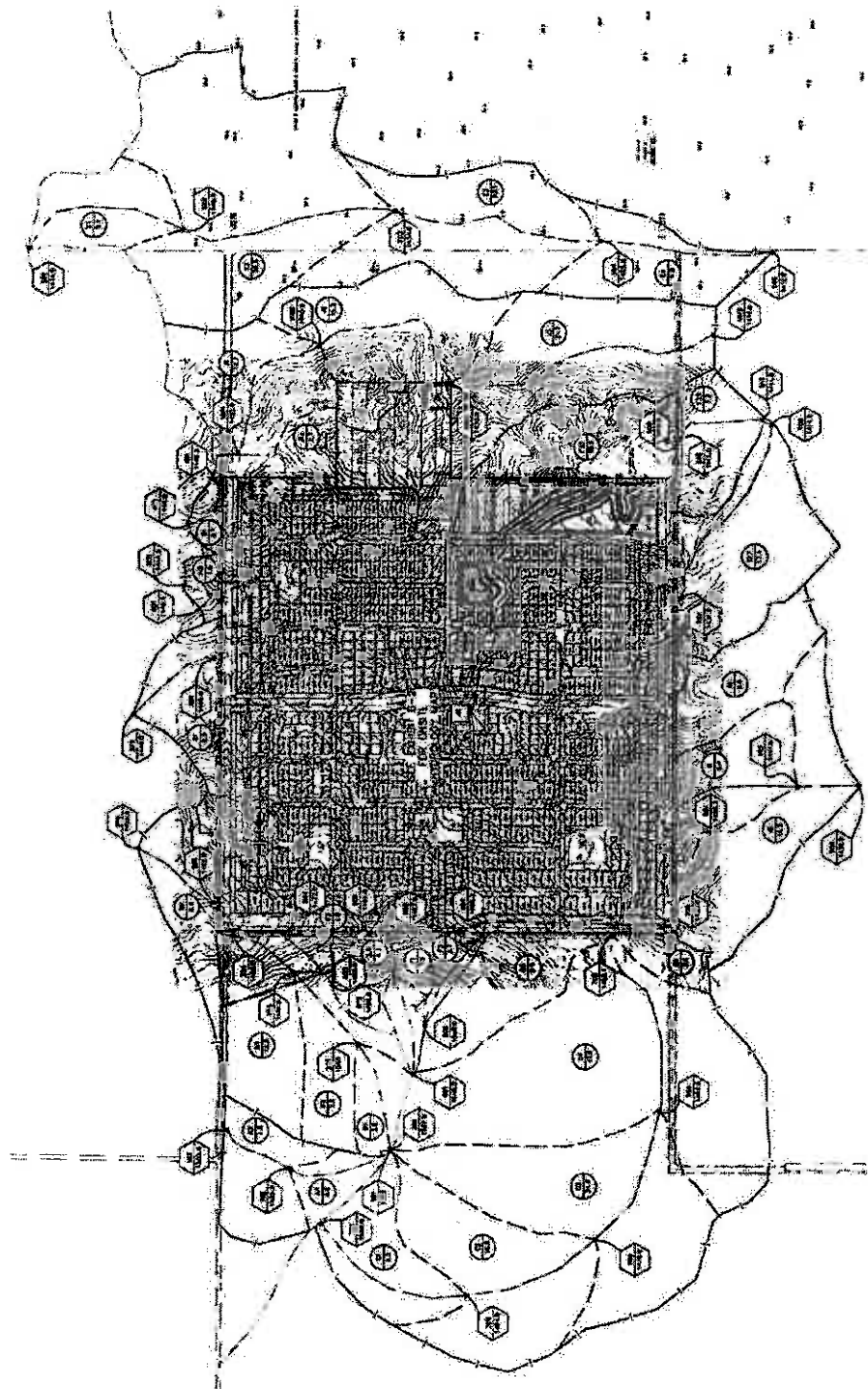
TTM 36785

PRE-PROJECT CONDITION
SITE HYDROLOGY MAP

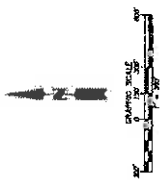
JCS Engineering & Consulting, Inc.
 3265 CALLE DE LOBO
 MURRIETA, CA 92562
 TEL 951.304.9553 FAX 951.304.3568

TENTATIVE TRACT MAP 36785 COUNTY OF RIVERSIDE, STATE OF CALIFORNIA POST-PROJECT CONDITION OFFSITE HYDROLOGY MAP

SHEET 1 OF 1



- LEGEND**
- 100' CONTOUR INTERVAL
 - APPROXIMATE REPORT ELEVATION
 - SUB-AREA PARCEL
 - FLOW DISTANCE
 - FLOW PATH
 - POST-PROJECT WATERSHED BOUNDARY
 - SANTA MARGARITA AND SANTA ANA RIVER DIVIDING WATERSHED BOUNDARY LINE
 - OFFSITE SANTA MARGARITA RIVER WATERSHED BOUNDARY
 - OFFSITE SANTA ANA RIVER WATERSHED BOUNDARY
 - 100' CONTOUR INTERVAL
 - SUB-BOUNDARY

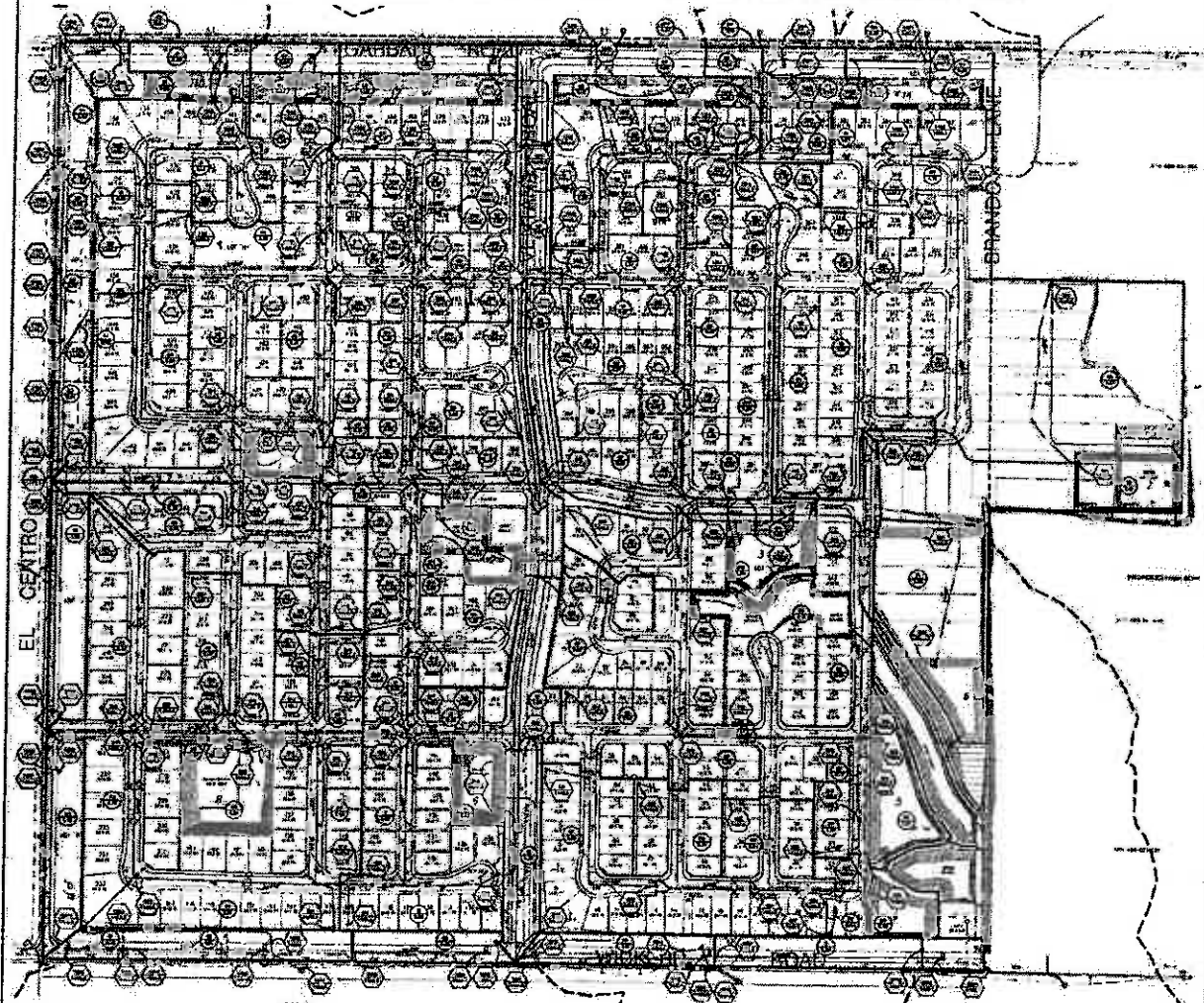


JCS
Engineering & Consulting, Inc.
3650 CALLE DE LOBO
MIRAFLORES, CA 92562
PH. 951.961.5557 FAX 951.961.5569

EXHIBIT 'B-1'
TTM 36875

**POST-PROJECT CONDITION
OFFSITE HYDROLOGY MAP**

TENTATIVE TRACT MAP 36785
COUNTY OF RIVERSIDE, STATE OF CALIFORNIA
POST PROJECT CONDITION - ON-SITE HYDROLOGY MAP



LEGEND

- PROPOSED ON-SITE DETENTION BASIN
- PROPOSED ON-SITE DETENTION SUB-DRAINAGE
- EXISTING UTILITY LINES AND OTHER INTERFERING SUB-STRUCTURE
- EXISTING UTILITY LINES AND OTHER INTERFERING SUB-STRUCTURE
- PROPOSED FLOW BASIN BOUNDARY LINE
- PROPOSED FLOW BASIN BOUNDARY LINE

PROPOSED ON-SITE DETENTION BASIN

PROPOSED ON-SITE DETENTION SUB-DRAINAGE

EXISTING UTILITY LINES AND OTHER INTERFERING SUB-STRUCTURE

PROPOSED FLOW BASIN BOUNDARY LINE



JG
JG & Associates, Inc.
3000 CALLE DE LOS RIOS
HOMEBRIDGE, CA 94620
PH 925.941.5502 FAX 925.941.5508

EXHIBIT "B-2"
TTM 36785
POST PROJECT CONDITION
ON-SITE HYDROLOGY MAP

Item 4.

Post-Project Flow Rate

Offsite Node 610-611	15.6
Offsite Node 609	27.3
Offsite Node 607	12.8
Offsite Node 604	2.9
Offsite Node 602-605	22
Onsite Node 409	28.3
Onsite Node 2004	5.2
Onsite Node 513	42.9
Onsite Node 602	12.8
Onsite Node 317	38.3
Onsite Node 225	44.1
Onsite node 118	42.6
Onsite Node 1709	2.5
Total Post-Project	297.3

A
Item 5.a.

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989 - 2005 Version 7.1
Rational Hydrology Study Date: 06/11/15 File:ARAPON100.out

TRACT MAP 36785
POST-PROJECT ON-SITE HYDROLOGY FOR AREA A
100-YEAR STORM EVENT
FILENAME: ARAPON100.RRV

***** Hydrology Study Control Information *****

English (in-lb) Units used in input data file

Program License Serial Number 6269

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2
2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.500(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.500(In/Hr)
Slope of intensity duration curve = 0.5500

Process from Point/Station 101.000 to Point/Station 102.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 997.000(Ft.)
Top (of initial area) elevation = 1469.800(Ft.)
Bottom (of initial area) elevation = 1454.100(Ft.)
Difference in elevation = 15.700(Ft.)
Slope = 0.01575 s(percent)= 1.57
TC = $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 14.161 min.
Rainfall intensity = 3.319(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.835
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.790
Decimal fraction soil group D = 0.210
RI index for soil(AMC 2) = 70.30
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 8.726(CFS)
Total initial stream area = 3.150(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 102.000 to Point/Station 105.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1453.100(Ft.)
Downstream point/station elevation = 1445.000(Ft.)
Pipe length = 47.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 8.726(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 8.726(CFS)
Normal flow depth in pipe = 6.63(In.)
Flow top width inside pipe = 11.93(In.)
Critical depth could not be calculated.
Pipe flow velocity = 19.61(Ft/s)
Travel time through pipe = 0.04 min.
Time of concentration (TC) = 14.20 min.

Process from Point/Station 102.000 to Point/Station 105.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
Stream flow area = 3.150(Ac.)
Runoff from this stream = 8.726(CFS)
Time of concentration = 14.20 min.
Rainfall intensity = 3.314(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 103.000 to Point/Station 104.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 601.000(Ft.)
Top (of initial area) elevation = 1465.700(Ft.)
Bottom (of initial area) elevation = 1458.300(Ft.)
Difference in elevation = 7.400(Ft.)
Slope = 0.01231 s(percent) = 1.23
TC = $k(0.390) * [(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 12.149 min.
Rainfall intensity = 3.611(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.836
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 5.705(CFS)
Total initial stream area = 1.890(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 104.000 to Point/Station 105.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1455.300(Ft.)
Downstream point/station elevation = 1445.000(Ft.)
Pipe length = 47.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 5.705(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 5.705(CFS)
Normal flow depth in pipe = 5.74(In.)
Flow top width inside pipe = 8.65(In.)
Critical depth could not be calculated.
Pipe flow velocity = 19.17(Ft/s)
Travel time through pipe = 0.04 min.
Time of concentration (TC) = 12.19 min.

Process from Point/Station 104.000 to Point/Station 105.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
Stream flow area = 1.890(Ac.)
Runoff from this stream = 5.705(CFS)
Time of concentration = 12.19 min.
Rainfall intensity = 3.604(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
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1	8.726	14.20	3.314
2	5.705	12.19	3.604

Largest stream flow has longer time of concentration

Qp = 8.726 + sum of
Qb Ia/Ib
5.705 * 0.919 = 5.245
Qp = 13.971

Total of 2 main streams to confluence:

Flow rates before confluence point:
8.726 5.705

Area of streams before confluence:
3.150 1.890

Results of confluence:

Total flow rate = 13.971(CFS)
Time of concentration = 14.201 min.
Effective stream area after confluence = 5.040(Ac.)

Process from Point/Station 105.000 to Point/Station 118.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1445.000(Ft.)
Downstream point/station elevation = 1444.000(Ft.)
Pipe length = 22.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 13.971(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 13.971(CFS)
Normal flow depth in pipe = 10.30(In.)
Flow top width inside pipe = 17.81(In.)
Critical Depth = 16.57(In.)
Pipe flow velocity = 13.37(Ft/s)
Travel time through pipe = 0.03 min.
Time of concentration (TC) = 14.23 min.

Process from Point/Station 105.000 to Point/Station 118.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
Stream flow area = 5.040(Ac.)
Runoff from this stream = 13.971(CFS)
Time of concentration = 14.23 min.
Rainfall intensity = 3.310(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 106.000 to Point/Station 107.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 571.000(Ft.)
Top (of initial area) elevation = 1472.700(Ft.)
Bottom (of initial area) elevation = 1451.100(Ft.)

Difference in elevation = 21.600(Ft.)
Slope = 0.03783 s(percent)= 3.78
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 9.509 min.
Rainfall intensity = 4.131(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.843
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 3.343(CFS)
Total initial stream area = 0.960(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 107.000 to Point/Station 118.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1451.100(Ft.)
Downstream point/station elevation = 1444.000(Ft.)
Pipe length = 207.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.343(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 3.343(CFS)
Normal flow depth in pipe = 6.05(In.)
Flow top width inside pipe = 12.00(In.)
Critical Depth = 9.38(In.)
Pipe flow velocity = 8.43(Ft/s)
Travel time through pipe = 0.41 min.
Time of concentration (TC) = 9.92 min.

Process from Point/Station 107.000 to Point/Station 118.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area = 0.960(Ac.)
Runoff from this stream = 3.343(CFS)
Time of concentration = 9.92 min.
Rainfall intensity = 4.037(In/Hr)
Program is now starting with Main Stream No. 3

Process from Point/Station 108.000 to Point/Station 110.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 965.000(Ft.)
Top (of initial area) elevation = 1466.500(Ft.)
Bottom (of initial area) elevation = 1451.900(Ft.)
Difference in elevation = 14.600(Ft.)
Slope = 0.01513 s(percent)= 1.51
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 14.090 min.
Rainfall intensity = 3.328(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.831
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 5.616(CFS)
Total initial stream area = 2.030(Ac.)

Pervious area fraction = 0.500

Process from Point/Station 108.000 to Point/Station 110.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 3 in normal stream number 1
Stream flow area = 2.030 (Ac.)
Runoff from this stream = 5.616 (CFS)
Time of concentration = 14.09 min.
Rainfall intensity = 3.328 (In/Hr)

Process from Point/Station 109.000 to Point/Station 110.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 719.000 (Ft.)
Top (of initial area) elevation = 1463.100 (Ft.)
Bottom (of initial area) elevation = 1451.900 (Ft.)
Difference in elevation = 11.200 (Ft.)
Slope = 0.01558 s (percent) = 1.56
TC = $k(0.390) * [(length^3) / (elevation\ change)]^{0.2}$
Initial area time of concentration = 12.453 min.
Rainfall intensity = 3.562 (In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.835
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil (AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 6.396 (CFS)
Total initial stream area = 2.150 (Ac.)
Pervious area fraction = 0.500

Process from Point/Station 109.000 to Point/Station 110.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 3 in normal stream number 2
Stream flow area = 2.150 (Ac.)
Runoff from this stream = 6.396 (CFS)
Time of concentration = 12.45 min.
Rainfall intensity = 3.562 (In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
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1	5.616	14.09	3.328
2	6.396	12.45	3.562

Largest stream flow has longer or shorter time of concentration

Qp = 6.396 + sum of
Qa Tb/Ta
5.616 * 0.884 = 4.964
Qp = 11.360

Total of 2 streams to confluence:
Flow rates before confluence point:
5.616 6.396
Area of streams before confluence:
2.030 2.150

Results of confluence:
Total flow rate = 11.360 (CFS)
Time of concentration = 12.453 min.
Effective stream area after confluence = 4.180 (Ac.)

Process from Point/Station 110.000 to Point/Station 111.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1451.900(Ft.)
End of street segment elevation = 1451.300(Ft.)
Length of street segment = 70.000(Ft.)
Height of curb above gutter flowline = 6.0(In.)
Width of half street (curb to crown) = 18.000(Ft.)
Distance from crown to crossfall grade break = 16.000(Ft.)
Slope from gutter to grade break (v/hz) = 0.020
Slope from grade break to crown (v/hz) = 0.020
Street flow is on (2) side(s) of the street
Distance from curb to property line = 10.000(Ft.)
Slope from curb to property line (v/hz) = 0.020
Gutter width = 2.000(Ft.)
Gutter hike from flowline = 2.000(In.)
Manning's N in gutter = 0.0150
Manning's N from gutter to grade break = 0.0150
Manning's N from grade break to crown = 0.0150
Estimated mean flow rate at midpoint of street = 11.781(CFS)
Depth of flow = 0.419(Ft.), Average velocity = 2.596(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width = 14.636(Ft.)
Flow velocity = 2.60(Ft/s)
Travel time = 0.45 min. TC = 12.90 min.
Adding area flow to street
USER INPUT of soil data for subarea
Runoff Coefficient = 0.834
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Rainfall intensity = 3.493(In/Hr) for a 100.0 year storm
Subarea runoff = 0.903(CFS) for 0.310(Ac.)
Total runoff = 12.263(CFS) Total area = 4.490(Ac.)
Street flow at end of street = 12.263(CFS)
Half street flow at end of street = 6.132(CFS)
Depth of flow = 0.424(Ft.), Average velocity = 2.621(Ft/s)
Flow width (from curb towards crown) = 14.874(Ft.)

Process from Point/Station 111.000 to Point/Station 118.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1448.300(Ft.)
Downstream point/station elevation = 1444.000(Ft.)
Pipe length = 58.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 12.263(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 12.263(CFS)
Normal flow depth in pipe = 9.22(In.)
Flow top width inside pipe = 14.60(In.)
Critical depth could not be calculated.
Pipe flow velocity = 15.49(Ft/s)
Travel time through pipe = 0.06 min.
Time of concentration (TC) = 12.96 min.

Process from Point/Station 111.000 to Point/Station 118.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 3
Stream flow area = 4.490(Ac.)

Runoff from this stream = 12.263(CFS)
Time of concentration = 12.96 min.
Rainfall intensity = 3.484(In/Hr)
Program is now starting with Main Stream No. 4

Process from Point/Station 112.000 to Point/Station 113.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 173.000(Ft.)
Top (of initial area) elevation = 1453.400(Ft.)
Bottom (of initial area) elevation = 1451.300(Ft.)
Difference in elevation = 2.100(Ft.)
Slope = 0.01214 s(percent)= 1.21
TC = $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 7.404 min.
Rainfall intensity = 4.741(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.850
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 3.101(CFS)
Total initial stream area = 0.770(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 113.000 to Point/Station 115.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1448.300(Ft.)
Downstream point/station elevation = 1447.300(Ft.)
Pipe length = 150.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.101(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 3.101(CFS)
Normal flow depth in pipe = 10.80(In.)
Flow top width inside pipe = 7.20(In.)
Critical Depth = 9.06(In.)
Pipe flow velocity = 4.16(Ft/s)
Travel time through pipe = 0.60 min.
Time of concentration (TC) = 8.00 min.

Process from Point/Station 113.000 to Point/Station 115.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 4 in normal stream number 1
Stream flow area = 0.770(Ac.)
Runoff from this stream = 3.101(CFS)
Time of concentration = 8.00 min.
Rainfall intensity = 4.542(In/Hr)

Process from Point/Station 114.000 to Point/Station 115.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 708.000(Ft.)
Top (of initial area) elevation = 1467.200(Ft.)
Bottom (of initial area) elevation = 1451.300(Ft.)
Difference in elevation = 15.900(Ft.)
Slope = 0.02246 s(percent)= 2.25
TC = $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 11.503 min.

Rainfall intensity = 3.721(In/Hr) for a 100.0 year storm
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.841
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.780
 Decimal fraction soil group D = 0.220
 RI index for soil(AMC 2) = 70.30
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Initial subarea runoff = 8.635(CFS)
 Total initial stream area = 2.760(Ac.)
 Pervious area fraction = 0.500

 Process from Point/Station 114.000 to Point/Station 115.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 4 in normal stream number 2
 Stream flow area = 2.760(Ac.)
 Runoff from this stream = 8.635(CFS)
 Time of concentration = 11.50 min.
 Rainfall intensity = 3.721(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	3.101	8.00	4.542
2	8.635	11.50	3.721

Largest stream flow has longer time of concentration

Qp = 8.635 + sum of
 $Q_b \cdot \frac{I_a}{I_b}$
 $3.101 * 0.819 = 2.541$
 Qp = 11.175

Total of 2 streams to confluence:
 Flow rates before confluence point:
 3.101 8.635

Area of streams before confluence:
 0.770 2.760

Results of confluence:

Total flow rate = 11.175(CFS)
 Time of concentration = 11.503 min.
 Effective stream area after confluence = 3.530(Ac.)

 Process from Point/Station 115.000 to Point/Station 117.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1447.300(Ft.)
 Downstream point/station elevation = 1446.300(Ft.)
 Pipe length = 150.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 11.175(CFS)
 Nearest computed pipe diameter = 21.00(In.)
 Calculated individual pipe flow = 11.175(CFS)
 Normal flow depth in pipe = 15.07(In.)
 Flow top width inside pipe = 18.91(In.)
 Critical Depth = 14.95(In.)
 Pipe flow velocity = 6.05(Ft/s)
 Travel time through pipe = 0.41 min.
 Time of concentration (TC) = 11.92 min.

 Process from Point/Station 115.000 to Point/Station 117.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 4 in normal stream number 1

Stream flow area = 3.530(Ac.)
 Runoff from this stream = 11.175(CFS)
 Time of concentration = 11.92 min.
 Rainfall intensity = 3.649(In/Hr)

 Process from Point/Station 116.000 to Point/Station 117.000
 **** INITIAL AREA EVALUATION ****

Initial area flow distance = 271.000(Ft.)
 Top (of initial area) elevation = 1454.100(Ft.)
 Bottom (of initial area) elevation = 1451.300(Ft.)
 Difference in elevation = 2.800(Ft.)
 Slope = 0.01033 s(percent)= 1.03
 $TC = k(0.390)*[(Length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 9.150 min.
 Rainfall intensity = 4.220(In/Hr) for a 100.0 year storm
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.848
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.740
 Decimal fraction soil group D = 0.260
 RI index for soil(AMC 2) = 70.60
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Initial subarea runoff = 3.649(CFS)
 Total initial stream area = 1.020(Ac.)
 Pervious area fraction = 0.500

 Process from Point/Station 116.000 to Point/Station 117.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 4 in normal stream number 2
 Stream flow area = 1.020(Ac.)
 Runoff from this stream = 3.649(CFS)
 Time of concentration = 9.15 min.
 Rainfall intensity = 4.220(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	11.175	11.92	3.649
2	3.649	9.15	4.220

Largest stream flow has longer time of concentration
 $Q_p = 11.175 + \text{sum of } \frac{Q_b \cdot I_a/I_b}{3.649 * 0.865} = 3.155$
 $Q_p = 14.331$

Total of 2 streams to confluence:
 Flow rates before confluence point:
 11.175 3.649
 Area of streams before confluence:
 3.530 1.020
 Results of confluence:
 Total flow rate = 14.331(CFS)
 Time of concentration = 11.916 min.
 Effective stream area after confluence = 4.550(Ac.)

 Process from Point/Station 117.000 to Point/Station 118.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1446.300(Ft.)
 Downstream point/station elevation = 1444.000(Ft.)

Pipe length = 178.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 14.331(CFS)
 Nearest computed pipe diameter = 21.00(In.)
 Calculated individual pipe flow = 14.331(CFS)
 Normal flow depth in pipe = 14.16(In.)
 Flow top width inside pipe = 19.69(In.)
 Critical Depth = 16.87(In.)
 Pipe flow velocity = 8.31(Ft/s)
 Travel time through pipe = 0.36 min.
 Time of concentration (TC) = 12.27 min.

 Process from Point/Station 117.000 to Point/Station 118.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 4
 Stream flow area = 4.550(Ac.)
 Runoff from this stream = 14.331(CFS)
 Time of concentration = 12.27 min.
 Rainfall intensity = 3.591(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	13.971	14.23	3.310
2	3.343	9.92	4.037
3	12.263	12.96	3.484
4	14.331	12.27	3.591

Largest stream flow has longer or shorter time of concentration

Qp = 14.331 + sum of
 Qa Tb/Ta
 13.971 * 0.863 = 12.050
 Qb Ia/Ib
 3.343 * 0.889 = 2.974
 Qa Tb/Ta
 12.263 * 0.947 = 11.609
 Qp = 40.964

Total of 4 main streams to confluence:

Flow rates before confluence point:

13.971	3.343	12.263	14.331
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Area of streams before confluence:

5.040	0.960	4.490	4.550
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Results of confluence:

Total flow rate = 40.964(CFS)
 Time of concentration = 12.273 min.
 Effective stream area after confluence = 15.040(Ac.)

 Process from Point/Station 118.000 to Point/Station 118.000
 **** SUBAREA FLOW ADDITION ****

USER INPUT of soil data for subarea

Runoff Coefficient = 0.771
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 RI index for soil(AMC 2) = 69.00
 Pervious area fraction = 1.000; Impervious fraction = 0.000
 Time of concentration = 12.27 min.
 Rainfall intensity = 3.591(In/Hr) for a 100.0 year storm
 Subarea runoff = 1.634(CFS) for 0.590(Ac.)
 Total runoff = 42.598(CFS) Total area = 15.630(Ac.)

End of computations, total study area = 15.63 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(A_p) = 0.519
Area averaged RI index number = 69.6

B
Item 5.b.

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989 - 2005 Version 7.1
Rational Hydrology Study Date: 06/11/15 File:ARBPON100.out

TRACT MAP 36785
POST-PROJECT ON-SITE HYDROLOGY FOR AREA B
100-YEAR STORM EVENT
FILENAME: ARBPON100.RRV

***** Hydrology Study Control Information *****

English (in-lb) Units used in input data file

Program License Serial Number 6269

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.500(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.500(In/Hr)
Slope of intensity duration curve = 0.5500

Process from Point/Station 201.000 to Point/Station 202.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 158.000(Ft.)
Top (of initial area) elevation = 1456.400(Ft.)
Bottom (of initial area) elevation = 1454.700(Ft.)
Difference in elevation = 1.700(Ft.)
Slope = 0.01076 s(percent) = 1.08
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 7.314 min.
Rainfall intensity = 4.773(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.850
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 3.002(CFS)
Total initial stream area = 0.740(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 202.000 to Point/Station 204.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1451.700(Ft.)
Downstream point/station elevation = 1451.100(Ft.)
Pipe length = 130.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 3.002 (CFS)
 Nearest computed pipe diameter = 15.00 (In.)
 Calculated individual pipe flow = 3.002 (CFS)
 Normal flow depth in pipe = 9.11 (In.)
 Flow top width inside pipe = 14.65 (In.)
 Critical Depth = 8.36 (In.)
 Pipe flow velocity = 3.85 (Ft/s)
 Travel time through pipe = 0.56 min.
 Time of concentration (TC) = 7.88 min.

 Process from Point/Station 202.000 to Point/Station 204.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
 Stream flow area = 0.740 (Ac.)
 Runoff from this stream = 3.002 (CFS)
 Time of concentration = 7.88 min.
 Rainfall intensity = 4.582 (In/Hr)
 Program is now starting with Main Stream No. 2

 Process from Point/Station 203.000 to Point/Station 204.000
 **** INITIAL AREA EVALUATION ****

Initial area flow distance = 166.000 (Ft.)
 Top (of initial area) elevation = 1456.500 (Ft.)
 Bottom (of initial area) elevation = 1454.500 (Ft.)
 Difference in elevation = 2.000 (Ft.)
 Slope = 0.01205 s (percent) = 1.20
 $TC = k(0.390) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 7.293 min.
 Rainfall intensity = 4.780 (In/Hr) for a 100.0 year storm
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.850
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 RI index for soil (AMC 2) = 69.00
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Initial subarea runoff = 3.128 (CFS)
 Total initial stream area = 0.770 (Ac.)
 Pervious area fraction = 0.500

 Process from Point/Station 203.000 to Point/Station 204.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Stream flow area = 0.770 (Ac.)
 Runoff from this stream = 3.128 (CFS)
 Time of concentration = 7.29 min.
 Rainfall intensity = 4.780 (In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	3.002	7.88	4.582
2	3.128	7.29	4.780

Largest stream flow has longer or shorter time of concentration

Qp = 3.128 + sum of
 $3.002 * \frac{Tb}{Ta} = 2.779$

Qp = 5.907

Total of 2 main streams to confluence:

Flow rates before confluence point:
3.002 3.128

Area of streams before confluence:
0.740 0.770

Results of confluence:

Total flow rate = 5.907(CFS)
Time of concentration = 7.293 min.
Effective stream area after confluence = 1.510(Ac.)

Process from Point/Station 204.000 to Point/Station 207.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1451.000(Ft.)
Downstream point/station elevation = 1449.400(Ft.)
Pipe length = 130.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 5.907(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 5.907(CFS)
Normal flow depth in pipe = 10.38(In.)
Flow top width inside pipe = 13.85(In.)
Critical Depth = 11.80(In.)
Pipe flow velocity = 6.52(Ft/s)
Travel time through pipe = 0.33 min.
Time of concentration (TC) = 7.63 min.

Process from Point/Station 204.000 to Point/Station 207.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
Stream flow area = 1.510(Ac.)
Runoff from this stream = 5.907(CFS)
Time of concentration = 7.63 min.
Rainfall intensity = 4.665(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 205.000 to Point/Station 206.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 344.000(Ft.)
Top (of initial area) elevation = 1459.900(Ft.)
Bottom (of initial area) elevation = 1454.400(Ft.)
Difference in elevation = 5.500(Ft.)
Slope = 0.01599 s(percent)= 1.60
TC = $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 9.224 min.
Rainfall intensity = 4.201(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.844
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 2.659(CFS)
Total initial stream area = 0.750(Ac.)
Pervious area fraction = 0.500

 Process from Point/Station 206.000 to Point/Station 207.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1452.400(Ft.)
 Downstream point/station elevation = 1449.400(Ft.)
 Pipe length = 73.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 2.659(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 2.659(CFS)
 Normal flow depth in pipe = 6.05(In.)
 Flow top width inside pipe = 8.45(In.)
 Critical Depth = 8.44(In.)
 Pipe flow velocity = 8.42(Ft/s)
 Travel time through pipe = 0.14 min.
 Time of concentration (TC) = 9.37 min.

 Process from Point/Station 206.000 to Point/Station 207.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Stream flow area = 0.750(Ac.)
 Runoff from this stream = 2.659(CFS)
 Time of concentration = 9.37 min.
 Rainfall intensity = 4.165(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	5.907	7.63	4.665
2	2.659	9.37	4.165

Largest stream flow has longer or shorter time of concentration

Qp = 5.907 + sum of

$$Q_a \quad T_b/T_a$$

$$2.659 * 0.814 = 2.164$$
 Qp = 8.072

Total of 2 main streams to confluence:

Flow rates before confluence point:

5.907 2.659

Area of streams before confluence:

1.510 0.750

Results of confluence:

Total flow rate = 8.072(CFS)

Time of concentration = 7.625 min.

Effective stream area after confluence = 2.260(Ac.)

 Process from Point/Station 207.000 to Point/Station 211.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1449.400(Ft.)
 Downstream point/station elevation = 1447.100(Ft.)
 Pipe length = 360.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 8.072(CFS)
 Nearest computed pipe diameter = 18.00(In.)
 Calculated individual pipe flow = 8.072(CFS)
 Normal flow depth in pipe = 14.16(In.)
 Flow top width inside pipe = 14.75(In.)
 Critical Depth = 13.20(In.)
 Pipe flow velocity = 5.41(Ft/s)
 Travel time through pipe = 1.11 min.
 Time of concentration (TC) = 8.73 min.

Process from Point/Station 207.000 to Point/Station 211.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
Stream flow area = 2.260(Ac.)
Runoff from this stream = 8.072(CFS)
Time of concentration = 8.73 min.
Rainfall intensity = 4.329(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 208.000 to Point/Station 210.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 590.000(Ft.)
Top (of initial area) elevation = 1460.000(Ft.)
Bottom (of initial area) elevation = 1451.300(Ft.)
Difference in elevation = 8.700(Ft.)
Slope = 0.01475 s(percent)= 1.47
TC = $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 11.632 min.
Rainfall intensity = 3.698(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.837
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 4.180(CFS)
Total initial stream area = 1.350(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 208.000 to Point/Station 210.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
Stream flow area = 1.350(Ac.)
Runoff from this stream = 4.180(CFS)
Time of concentration = 11.63 min.
Rainfall intensity = 3.698(In/Hr)

Process from Point/Station 209.000 to Point/Station 210.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 393.000(Ft.)
Top (of initial area) elevation = 1455.300(Ft.)
Bottom (of initial area) elevation = 1451.300(Ft.)
Difference in elevation = 4.000(Ft.)
Slope = 0.01018 s(percent)= 1.02
TC = $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 10.648 min.
Rainfall intensity = 3.882(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.840
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500

Initial subarea runoff = 6.456(CFS)
 Total initial stream area = 1.980(Ac.)
 Pervious area fraction = 0.500

 Process from Point/Station 209.000 to Point/Station 210.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
 Stream flow area = 1.980(Ac.)
 Runoff from this stream = 6.456(CFS)
 Time of concentration = 10.65 min.
 Rainfall intensity = 3.882(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	4.180	11.63	3.698
2	6.456	10.65	3.882

Largest stream flow has longer or shorter time of concentration

Qp = 6.456 + sum of
 $Q_a \cdot T_b / T_a$
 $4.180 * 0.915 = 3.826$
 Qp = 10.282

Total of 2 streams to confluence:
 Flow rates before confluence point:
 4.180 6.456

Area of streams before confluence:
 1.350 1.980

Results of confluence:

Total flow rate = 10.282(CFS)
 Time of concentration = 10.648 min.
 Effective stream area after confluence = 3.330(Ac.)

 Process from Point/Station 210.000 to Point/Station 211.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1451.300(Ft.)
 End of street segment elevation = 1450.100(Ft.)
 Length of street segment = 98.000(Ft.)
 Height of curb above gutter flowline = 6.0(In.)
 Width of half street (curb to crown) = 18.000(Ft.)
 Distance from crown to crossfall grade break = 16.000(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 2.000(Ft.)
 Gutter hike from flowline = 2.000(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 11.193(CFS)
 Depth of flow = 0.393(Ft.), Average velocity = 2.937(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 13.337(Ft.)
 Flow velocity = 2.94(Ft/s)
 Travel time = 0.56 min. TC = 11.20 min.
 Adding area flow to street
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.838
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000

Decimal fraction soil group D = 0.000
 RI index for soil(AMC 2) = 69.00
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Rainfall intensity = 3.775(In/Hr) for a 100.0 year storm
 Subarea runoff = 1.867(CFS) for 0.590(Ac.)
 Total runoff = 12.149(CFS) Total area = 3.920(Ac.)
 Street flow at end of street = 12.149(CFS)
 Half street flow at end of street = 6.074(CFS)
 Depth of flow = 0.402(Ft.), Average velocity = 2.995(Ft/s)
 Flow width (from curb towards crown)= 13.789(Ft.)

 Process from Point/Station 210.000 to Point/Station 211.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Stream flow area = 3.920(Ac.)
 Runoff from this stream = 12.149(CFS)
 Time of concentration = 11.20 min.
 Rainfall intensity = 3.775(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	8.072	8.73	4.329
2	12.149	11.20	3.775

Largest stream flow has longer time of concentration
 $Q_p = 12.149 + \text{sum of } Q_b \text{ Ia/Ib}$
 $8.072 * 0.872 = 7.038$
 $Q_p = 19.187$

Total of 2 main streams to confluence:
 Flow rates before confluence point:
 8.072 12.149
 Area of streams before confluence:
 2.260 3.920

Results of confluence:
 Total flow rate = 19.187(CFS)
 Time of concentration = 11.205 min.
 Effective stream area after confluence = 6.180(Ac.)

 Process from Point/Station 211.000 to Point/Station 213.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1447.100(Ft.)
 Downstream point/station elevation = 1446.000(Ft.)
 Pipe length = 158.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 19.187(CFS)
 Nearest computed pipe diameter = 24.00(In.)
 Calculated individual pipe flow = 19.187(CFS)
 Normal flow depth in pipe = 20.06(In.)
 Flow top width inside pipe = 17.78(In.)
 Critical Depth = 18.90(In.)
 Pipe flow velocity = 6.84(Ft/s)
 Travel time through pipe = 0.38 min.
 Time of concentration (TC) = 11.59 min.

 Process from Point/Station 211.000 to Point/Station 213.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
 In Main Stream number: 1
 Stream flow area = 6.180(Ac.)
 Runoff from this stream = 19.187(CFS)
 Time of concentration = 11.59 min.
 Rainfall intensity = 3.705(In/Hr)
 Program is now starting with Main Stream No. 2

 Process from Point/Station 212.000 to Point/Station 213.000
 **** INITIAL AREA EVALUATION ****

Initial area flow distance = 80.000(Ft.)
 Top (of initial area) elevation = 1450.800(Ft.)
 Bottom (of initial area) elevation = 1450.000(Ft.)
 Difference in elevation = 0.800(Ft.)
 Slope = 0.01000 s(percent) = 1.00
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 5.653 min.
 Rainfall intensity = 5.499(In/Hr) for a 100.0 year storm
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.856
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 RI index for soil(AMC 2) = 69.00
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Initial subarea runoff = 0.706(CFS)
 Total initial stream area = 0.150(Ac.)
 Pervious area fraction = 0.500

 Process from Point/Station 212.000 to Point/Station 213.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
 In Main Stream number: 2
 Stream flow area = 0.150(Ac.)
 Runoff from this stream = 0.706(CFS)
 Time of concentration = 5.65 min.
 Rainfall intensity = 5.499(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	19.187	11.59	3.705
2	0.706	5.65	5.499

Largest stream flow has longer time of concentration
 $Q_p = 19.187 + \text{sum of } Q_b \text{ Ia/Ib}$
 $0.706 * 0.674 = 0.476$
 $Q_p = 19.663$

Total of 2 main streams to confluence:
 Flow rates before confluence point:
 19.187 0.706
 Area of streams before confluence:
 6.180 0.150

Results of confluence:
 Total flow rate = 19.663(CFS)
 Time of concentration = 11.589 min.
 Effective stream area after confluence = 6.330(Ac.)

Process from Point/Station 213.000 to Point/Station 216.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1446.000(Ft.)
Downstream point/station elevation = 1445.500(Ft.)
Pipe length = 40.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 19.663(CFS)
Nearest computed pipe diameter = 24.00(In.)
Calculated individual pipe flow = 19.663(CFS)
Normal flow depth in pipe = 15.91(In.)
Flow top width inside pipe = 22.69(In.)
Critical Depth = 19.13(In.)
Pipe flow velocity = 8.90(Ft/s)
Travel time through pipe = 0.07 min.
Time of concentration (TC) = 11.66 min.

Process from Point/Station 213.000 to Point/Station 216.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area = 6.330(Ac.)
Runoff from this stream = 19.663(CFS)
Time of concentration = 11.66 min.
Rainfall intensity = 3.692(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 214.000 to Point/Station 215.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 240.000(Ft.)
Top (of initial area) elevation = 1452.400(Ft.)
Bottom (of initial area) elevation = 1452.000(Ft.)
Difference in elevation = 0.400(Ft.)
Slope = 0.00167 s(percent) = 0.17
TC = $k(0.390)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$
Initial area time of concentration = 12.554 min.
Rainfall intensity = 3.546(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.835
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 2.813(CFS)
Total initial stream area = 0.950(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 215.000 to Point/Station 216.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1449.000(Ft.)
Downstream point/station elevation = 1445.500(Ft.)
Pipe length = 99.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.813(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 2.813(CFS)
Normal flow depth in pipe = 6.70(In.)
Flow top width inside pipe = 7.85(In.)
Critical Depth = 8.54(In.)
Pipe flow velocity = 7.97(Ft/s)
Travel time through pipe = 0.21 min.

Time of concentration (TC) = 12.76 min.

Process from Point/Station 215.000 to Point/Station 216.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
Stream flow area = 0.950(Ac.)
Runoff from this stream = 2.813(CFS)
Time of concentration = 12.76 min.
Rainfall intensity = 3.514(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	19.663	11.66	3.692
2	2.813	12.76	3.514

Largest stream flow has longer or shorter time of concentration

Qp = 19.663 + sum of
Qa Tb/Ta
2.813 * 0.914 = 2.571
Qp = 22.234

Total of 2 main streams to confluence:

Flow rates before confluence point:

19.663 2.813

Area of streams before confluence:

6.330 0.950

Results of confluence:

Total flow rate = 22.234(CFS)

Time of concentration = 11.664 min.

Effective stream area after confluence = 7.280(Ac.)

Process from Point/Station 216.000 to Point/Station 225.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1445.500(Ft.)
Downstream point/station elevation = 1440.000(Ft.)
Pipe length = 180.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 22.234(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 22.234(CFS)
Normal flow depth in pipe = 14.25(In.)
Flow top width inside pipe = 19.62(In.)
Critical Depth = 19.70(In.)
Pipe flow velocity = 12.80(Ft/s)
Travel time through pipe = 0.23 min.
Time of concentration (TC) = 11.90 min.

Process from Point/Station 216.000 to Point/Station 225.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
Stream flow area = 7.280(Ac.)
Runoff from this stream = 22.234(CFS)
Time of concentration = 11.90 min.
Rainfall intensity = 3.652(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 217.000 to Point/Station 218.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 451.000(Ft.)
Top (of initial area) elevation = 1451.200(Ft.)
Bottom (of initial area) elevation = 1447.000(Ft.)
Difference in elevation = 4.200(Ft.)
Slope = 0.00931 s(percent)= 0.93
TC = $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 11.453 min.
Rainfall intensity = 3.730(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.838
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 6.218(CFS)
Total initial stream area = 1.990(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 218.000 to Point/Station 220.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1444.000(Ft.)
Downstream point/station elevation = 1443.000(Ft.)
Pipe length = 154.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 6.218(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 6.218(CFS)
Normal flow depth in pipe = 11.46(In.)
Flow top width inside pipe = 17.31(In.)
Critical Depth = 11.57(In.)
Pipe flow velocity = 5.23(Ft/s)
Travel time through pipe = 0.49 min.
Time of concentration (TC) = 11.94 min.

Process from Point/Station 218.000 to Point/Station 220.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
Stream flow area = 1.990(Ac.)
Runoff from this stream = 6.218(CFS)
Time of concentration = 11.94 min.
Rainfall intensity = 3.645(In/Hr)

Process from Point/Station 219.000 to Point/Station 220.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 180.000(Ft.)
Top (of initial area) elevation = 1449.800(Ft.)
Bottom (of initial area) elevation = 1447.000(Ft.)
Difference in elevation = 2.800(Ft.)
Slope = 0.01556 s(percent)= 1.56
TC = $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 7.158 min.
Rainfall intensity = 4.830(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.850
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000
 RI index for soil(AMC 2) = 69.00
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Initial subarea runoff = 3.245(CFS)
 Total initial stream area = 0.790(Ac.)
 Pervious area fraction = 0.500

++++++
 Process from Point/Station 219.000 to Point/Station 220.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
 Stream flow area = 0.790(Ac.)
 Runoff from this stream = 3.245(CFS)
 Time of concentration = 7.16 min.
 Rainfall intensity = 4.830(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
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1	6.218	11.94	3.645
2	3.245	7.16	4.830

Largest stream flow has longer time of concentration

$Q_p = 6.218 + \text{sum of}$
 $Q_b \quad I_a/I_b$
 $3.245 * 0.755 = 2.448$
 $Q_p = 8.666$

Total of 2 streams to confluence:
 Flow rates before confluence point:
 6.218 3.245

Area of streams before confluence:
 1.990 0.790

Results of confluence:

Total flow rate = 8.666(CFS)
 Time of concentration = 11.943 min.
 Effective stream area after confluence = 2.780(Ac.)

++++++
 Process from Point/Station 220.000 to Point/Station 222.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1443.000(Ft.)
 Downstream point/station elevation = 1442.000(Ft.)
 Pipe length = 140.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 8.666(CFS)
 Nearest computed pipe diameter = 18.00(In.)
 Calculated individual pipe flow = 8.666(CFS)
 Normal flow depth in pipe = 14.39(In.)
 Flow top width inside pipe = 14.41(In.)
 Critical Depth = 13.68(In.)
 Pipe flow velocity = 5.73(Ft/s)
 Travel time through pipe = 0.41 min.
 Time of concentration (TC) = 12.35 min.

++++++
 Process from Point/Station 220.000 to Point/Station 222.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
 Stream flow area = 2.780(Ac.)
 Runoff from this stream = 8.666(CFS)
 Time of concentration = 12.35 min.
 Rainfall intensity = 3.578(In/Hr)

 Process from Point/Station 221.000 to Point/Station 222.000
 **** INITIAL AREA EVALUATION ****

Initial area flow distance = 231.000(Ft.)
 Top (of initial area) elevation = 1450.300(Ft.)
 Bottom (of initial area) elevation = 1447.000(Ft.)
 Difference in elevation = 3.300(Ft.)
 Slope = 0.01429 s(percent)= 1.43
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 8.045 min.
 Rainfall intensity = 4.529(In/Hr) for a 100.0 year storm
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.847
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 RI index for soil(AMC 2) = 69.00
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Initial subarea runoff = 3.570(CFS)
 Total initial stream area = 0.930(Ac.)
 Pervious area fraction = 0.500

 Process from Point/Station 221.000 to Point/Station 222.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
 Stream flow area = 0.930(Ac.)
 Runoff from this stream = 3.570(CFS)
 Time of concentration = 8.05 min.
 Rainfall intensity = 4.529(In/Rr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	8.666	12.35	3.578
2	3.570	8.05	4.529

Largest stream flow has longer time of concentration

Qp = 8.666 + sum of
 Qb Ia/Ib
 3.570 * 0.790 = 2.820
 Qp = 11.486

Total of 2 streams to confluence:
 Flow rates before confluence point:
 8.666 3.570

Area of streams before confluence:
 2.780 0.930

Results of confluence:
 Total flow rate = 11.486(CFS)
 Time of concentration = 12.351 min.
 Effective stream area after confluence = 3.710(Ac.)

 Process from Point/Station 222.000 to Point/Station 225.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1442.000(Ft.)
 Downstream point/station elevation = 1440.000(Ft.)
 Pipe length = 102.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 11.486(CFS)
 Nearest computed pipe diameter = 18.00(In.)
 Calculated individual pipe flow = 11.486(CFS)
 Normal flow depth in pipe = 11.96(In.)
 Flow top width inside pipe = 17.00(In.)

Critical Depth = 15.51(In.)
Pipe flow velocity = 9.21(Ft/s)
Travel time through pipe = 0.18 min.
Time of concentration (TC) = 12.54 min.

Process from Point/Station 222.000 to Point/Station 225.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
Stream flow area = 3.710(Ac.)
Runoff from this stream = 11.486(CFS)
Time of concentration = 12.54 min.
Rainfall intensity = 3.549(In/Hr)
Program is now starting with Main Stream No. 3

Process from Point/Station 223.000 to Point/Station 224.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 637.000(Ft.)
Top (of initial area) elevation = 1456.500(Ft.)
Bottom (of initial area) elevation = 1446.100(Ft.)
Difference in elevation = 10.400(Ft.)
Slope = 0.01633 s(percent) = 1.63
TC = $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 11.753 min.
Rainfall intensity = 3.677(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.837
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 8.432(CFS)
Total initial stream area = 2.740(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 224.000 to Point/Station 225.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1443.100(Ft.)
Downstream point/station elevation = 1440.000(Ft.)
Pipe length = 239.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 8.432(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 8.432(CFS)
Normal flow depth in pipe = 11.14(In.)
Flow top width inside pipe = 17.48(In.)
Critical Depth = 13.49(In.)
Pipe flow velocity = 7.33(Ft/s)
Travel time through pipe = 0.54 min.
Time of concentration (TC) = 12.30 min.

Process from Point/Station 224.000 to Point/Station 225.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 3
Stream flow area = 2.740(Ac.)
Runoff from this stream = 8.432(CFS)
Time of concentration = 12.30 min.

Rainfall intensity = 3.587(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	22.234	11.90	3.652
2	11.486	12.54	3.549
3	8.432	12.30	3.587

Largest stream flow has longer or shorter time of concentration

Qp = 22.234 + sum of
 Qa Tb/Ta
 11.486 * 0.949 = 10.902
 Qa Tb/Ta
 8.432 * 0.968 = 8.160
 Qp = 41.296

Total of 3 main streams to confluence:

Flow rates before confluence point:
 22.234 11.486 8.432
 Area of streams before confluence:
 7.280 3.710 2.740

Results of confluence:

Total flow rate = 41.296(CFS)
 Time of concentration = 11.899 min.
 Effective stream area after confluence = 13.730(Ac.)

 Process from Point/Station 225.000 to Point/Station 225.000
 **** SUBAREA FLOW ADDITION ****

USER INPUT of soil data for subarea

Runoff Coefficient = 0.773
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 RI index for soil(AMC 2) = 69.00
 Pervious area fraction = 1.000; Impervious fraction = 0.000
 Time of concentration = 11.90 min.
 Rainfall intensity = 3.652(In/Hr) for a 100.0 year storm
 Subarea runoff = 2.796(CFS) for 0.990(Ac.)
 Total runoff = 44.092(CFS) Total area = 14.720(Ac.)
 End of computations, total study area = 14.72 (Ac.)
 The following figures may
 be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.534
 Area averaged RI index number = 69.0

C
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Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989 - 2005 Version 7.1
Rational Hydrology Study Date: 06/11/15 File:ARCPON100.out

TRACT MAP 36785
POST-PROJECT ON-SITE HYDROLOGY FOR AREA c
100-YEAR STORM EVENT
FILENAME: ARCPON100.RRV

***** Hydrology Study Control Information *****

English (in-lb) Units used in input data file

Program License Serial Number 6269

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.500(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.500(In/Hr)
Slope of intensity duration curve = 0.5500

Process from Point/Station 301.000 to Point/Station 302.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 434.000(Ft.)
Top (of initial area) elevation = 1458.600(Ft.)
Bottom (of initial area) elevation = 1453.400(Ft.)
Difference in elevation = 5.200(Ft.)
Slope = 0.01198 s(percent)= 1.20
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.724 min.
Rainfall intensity = 3.867(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.840
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 3.474(CFS)
Total initial stream area = 1.070(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 302.000 to Point/Station 304.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1458.600(Ft.)
End of street segment elevation = 1446.000(Ft.)
Length of street segment = 290.000(Ft.)

Height of curb above gutter flowline = 6.0(In.)
 Width of half street (curb to crown) = 18.000(Ft.)
 Distance from crown to crossfall grade break = 16.000(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 2.000(Ft.)
 Gutter hike from flowline = 2.000(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 5.128(CFS)
 Depth of flow = 0.270(Ft.), Average velocity = 4.019(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 7.150(Ft.)
 Flow velocity = 4.02(Ft/s)
 Travel time = 1.20 min. TC = 11.93 min.
 Adding area flow to street
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.837
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 RI index for soil(AMC 2) = 69.00
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Rainfall intensity = 3.647(In/Hr) for a 100.0 year storm
 Subarea runoff = 3.204(CFS) for 1.050(Ac.)
 Total runoff = 6.678(CFS) Total area = 2.120(Ac.)
 Street flow at end of street = 6.678(CFS)
 Half street flow at end of street = 3.339(CFS)
 Depth of flow = 0.289(Ft.), Average velocity = 4.250(Ft/s)
 Flow width (from curb towards crown) = 8.118(Ft.)

++++++
 Process from Point/Station 302.000 to Point/Station 304.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
 Stream flow area = 2.120(Ac.)
 Runoff from this stream = 6.678(CFS)
 Time of concentration = 11.93 min.
 Rainfall intensity = 3.647(In/Hr)
 Program is now starting with Main Stream No. 2

++++++
 Process from Point/Station 303.000 to Point/Station 304.000
 **** INITIAL AREA EVALUATION ****

Initial area flow distance = 455.000(Ft.)
 Top (of initial area) elevation = 1451.500(Ft.)
 Bottom (of initial area) elevation = 1446.000(Ft.)
 Difference in elevation = 5.500(Ft.)
 Slope = 0.01209 s(percent) = 1.21
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 10.909 min.
 Rainfall intensity = 3.831(In/Hr) for a 100.0 year storm
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.839
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 RI index for soil(AMC 2) = 69.00
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Initial subarea runoff = 7.297(CFS)

Total initial stream area = 2.270(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 303.000 to Point/Station 304.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
Stream flow area = 2.270(Ac.)
Runoff from this stream = 7.297(CFS)
Time of concentration = 10.91 min.
Rainfall intensity = 3.831(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	6.678	11.93	3.647
2	7.297	10.91	3.831

Largest stream flow has longer or shorter time of concentration

Qp = 7.297 + sum of
Qa Tb/Ta
6.678 * 0.915 = 6.108
Qp = 13.405

Total of 2 main streams to confluence:

Flow rates before confluence point:

6.678 7.297

Area of streams before confluence:

2.120 2.270

Results of confluence:

Total flow rate = 13.405(CFS)

Time of concentration = 10.909 min.

Effective stream area after confluence = 4.390(Ac.)

Process from Point/Station 304.000 to Point/Station 305.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1446.000(Ft.)
End of street segment elevation = 1444.400(Ft.)
Length of street segment = 434.000(Ft.)
Height of curb above gutter flowline = 6.0(In.)
Width of half street (curb to crown) = 18.000(Ft.)
Distance from crown to crossfall grade break = 16.000(Ft.)
Slope from gutter to grade break (v/hz) = 0.020
Slope from grade break to crown (v/hz) = 0.020
Street flow is on (2) side(s) of the street
Distance from curb to property line = 10.000(Ft.)
Slope from curb to property line (v/hz) = 0.020
Gutter width = 2.000(Ft.)
Gutter hike from flowline = 2.000(In.)
Manning's N in gutter = 0.0150
Manning's N from gutter to grade break = 0.0150
Manning's N from grade break to crown = 0.0150
Estimated mean flow rate at midpoint of street = 14.093(CFS)
Depth of flow = 0.496(Ft.), Average velocity = 1.994(Ft/s)
Note: depth of flow exceeds top of street crown.
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width = 18.000(Ft.)
Flow velocity = 1.99(Ft/s)
Travel time = 3.63 min. TC = 14.54 min.
Adding area flow to street
USER INPUT of soil data for subarea
Runoff Coefficient = 0.830

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Rainfall intensity = 3.271(In/Hr) for a 100.0 year storm
Subarea runoff = 1.222(CFS) for 0.450(Ac.)
Total runoff = 14.628(CFS) Total area = 4.840(Ac.)
Street flow at end of street = 14.628(CFS)
Half street flow at end of street = 7.314(CFS)
Depth of flow = 0.500(Ft.), Average velocity = 2.023(Ft/s)
Warning: depth of flow exceeds top of curb
Note: depth of flow exceeds top of street crown.
Distance that curb overflow reaches into property = 0.02(Ft.)
Flow width (from curb towards crown) = 18.000(Ft.)

Process from Point/Station 305.000 to Point/Station 308.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1441.400(Ft.)
Downstream point/station elevation = 1438.000(Ft.)
Pipe length = 315.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 14.628(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 14.628(CFS)
Normal flow depth in pipe = 15.42(In.)
Flow top width inside pipe = 18.55(In.)
Critical Depth = 17.01(In.)
Pipe flow velocity = 7.73(Ft/s)
Travel time through pipe = 0.68 min.
Time of concentration (TC) = 15.22 min.

Process from Point/Station 305.000 to Point/Station 308.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area = 4.840(Ac.)
Runoff from this stream = 14.628(CFS)
Time of concentration = 15.22 min.
Rainfall intensity = 3.190(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 306.000 to Point/Station 307.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 532.000(Ft.)
Top (of initial area) elevation = 1448.000(Ft.)
Bottom (of initial area) elevation = 1441.200(Ft.)
Difference in elevation = 6.800(Ft.)
Slope = 0.01278 s(percent) = 1.28
TC = $k(0.390) * [(length^3) / (elevation\ change)]^{0.2}$
Initial area time of concentration = 11.484 min.
Rainfall intensity = 3.724(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.838
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 7.923(CFS)
Total initial stream area = 2.540(Ac.)

Pervious area fraction = 0.500

Process from Point/Station 307.000 to Point/Station 308.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1439.200(Ft.)
Downstream point/station elevation = 1438.000(Ft.)
Pipe length = 112.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 7.923(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 7.923(CFS)
Normal flow depth in pipe = 11.40(In.)
Flow top width inside pipe = 17.35(In.)
Critical Depth = 13.09(In.)
Pipe flow velocity = 6.71(Ft/s)
Travel time through pipe = 0.28 min.
Time of concentration (TC) = 11.76 min.

Process from Point/Station 307.000 to Point/Station 308.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
Stream flow area = 2.540(Ac.)
Runoff from this stream = 7.923(CFS)
Time of concentration = 11.76 min.
Rainfall intensity = 3.675(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	14.628	15.22	3.190
2	7.923	11.76	3.675

Largest stream flow has longer time of concentration

Qp = 14.628 + sum of
Qb Ia/Ib
7.923 * 0.868 = 6.878
Qp = 21.505

Total of 2 main streams to confluence:

Flow rates before confluence point:
14.628 7.923
Area of streams before confluence:
4.840 2.540

Results of confluence:

Total flow rate = 21.505(CFS)
Time of concentration = 15.215 min.
Effective stream area after confluence = 7.380(Ac.)

Process from Point/Station 308.000 to Point/Station 314.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1438.000(Ft.)
Downstream point/station elevation = 1437.000(Ft.)
Pipe length = 90.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 21.505(CFS)
Nearest computed pipe diameter = 24.00(In.)
Calculated individual pipe flow = 21.505(CFS)
Normal flow depth in pipe = 17.84(In.)
Flow top width inside pipe = 20.97(In.)
Critical Depth = 19.89(In.)

Pipe flow velocity = 8.59(Ft/s)
Travel time through pipe = 0.17 min.
Time of concentration (TC) = 15.39 min.

Process from Point/Station 308.000 to Point/Station 314.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area = 7.380(Ac.)
Runoff from this stream = 21.505(CFS)
Time of concentration = 15.39 min.
Rainfall intensity = 3.170(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 309.000 to Point/Station 310.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 767.000(Ft.)
Top (of initial area) elevation = 1458.600(Ft.)
Bottom (of initial area) elevation = 1447.000(Ft.)
Difference in elevation = 11.600(Ft.)
Slope = 0.01512 s(percent) = 1.51
TC = $k(0.390)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$
Initial area time of concentration = 12.854 min.
Rainfall intensity = 3.500(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.834
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 3.037(CFS)
Total initial stream area = 1.040(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 310.000 to Point/Station 312.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1447.000(Ft.)
End of street segment elevation = 1442.200(Ft.)
Length of street segment = 397.000(Ft.)
Height of curb above gutter flowline = 6.0(In.)
Width of half street (curb to crown) = 18.000(Ft.)
Distance from crown to crossfall grade break = 16.000(Ft.)
Slope from gutter to grade break (v/hz) = 0.020
Slope from grade break to crown (v/hz) = 0.020
Street flow is on (2) side(s) of the street
Distance from curb to property line = 10.000(Ft.)
Slope from curb to property line (v/hz) = 0.020
Gutter width = 2.000(Ft.)
Gutter hike from flowline = 2.000(In.)
Manning's N in gutter = 0.0150
Manning's N from gutter to grade break = 0.0150
Manning's N from grade break to crown = 0.0150
Estimated mean flow rate at midpoint of street = 4.168(CFS)
Depth of flow = 0.302(Ft.), Average velocity = 2.326(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width = 8.771(Ft.)
Flow velocity = 2.33(Ft/s)
Travel time = 2.84 min. TC = 15.70 min.
Adding area flow to street
USER INPUT of soil data for subarea

Runoff Coefficient = 0.828
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 RI index for soil(AMC 2) = 69.00
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Rainfall intensity = 3.136(In/Hr) for a 100.0 year storm
 Subarea runoff = 2.129(CFS) for 0.820(Ac.)
 Total runoff = 5.165(CFS) Total area = 1.860(Ac.)
 Street flow at end of street = 5.165(CFS)
 Half street flow at end of street = 2.583(CFS)
 Depth of flow = 0.320(Ft.), Average velocity = 2.440(Ft/s)
 Flow width (from curb towards crown)= 9.652(Ft.)

 Process from Point/Station 310.000 to Point/Station 312.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
 Stream flow area = 1.860(Ac.)
 Runoff from this stream = 5.165(CFS)
 Time of concentration = 15.70 min.
 Rainfall intensity = 3.136(In/Hr)

 Process from Point/Station 311.000 to Point/Station 312.000
 **** INITIAL AREA EVALUATION ****

Initial area flow distance = 335.000(Ft.)
 Top (of initial area) elevation = 1445.900(Ft.)
 Bottom (of initial area) elevation = 1442.200(Ft.)
 Difference in elevation = 3.700(Ft.)
 Slope = 0.01104 s(percent)= 1.10
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 9.828 min.
 Rainfall intensity = 4.057(In/Hr) for a 100.0 year storm
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.842
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 RI index for soil(AMC 2) = 69.00
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Initial subarea runoff = 3.382(CFS)
 Total initial stream area = 0.990(Ac.)
 Pervious area fraction = 0.500

 Process from Point/Station 311.000 to Point/Station 312.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
 Stream flow area = 0.990(Ac.)
 Runoff from this stream = 3.382(CFS)
 Time of concentration = 9.83 min.
 Rainfall intensity = 4.057(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	5.165	15.70	3.136
2	3.382	9.83	4.057

Largest stream flow has longer time of concentration
 $Q_p = 5.165 + \text{sum of}$

Qb Ia/Ib
 3.382 * 0.773 = 2.614
 Qp = 7.780

Total of 2 streams to confluence:
 Flow rates before confluence point:
 5.165 3.382
 Area of streams before confluence:
 1.860 0.990
 Results of confluence:
 Total flow rate = 7.780 (CFS)
 Time of concentration = 15.699 min.
 Effective stream area after confluence = 2.850 (Ac.)

++++++
 Process from Point/Station 312.000 to Point/Station 314.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1442.200 (Ft.)
 End of street segment elevation = 1441.000 (Ft.)
 Length of street segment = 131.000 (Ft.)
 Height of curb above gutter flowline = 6.0 (In.)
 Width of half street (curb to crown) = 18.000 (Ft.)
 Distance from crown to crossfall grade break = 16.000 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 2.000 (Ft.)
 Gutter hike from flowline = 2.000 (In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 8.530 (CFS)
 Depth of flow = 0.380 (Ft.), Average velocity = 2.465 (Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 12.663 (Ft.)
 Flow velocity = 2.47 (Ft/s)
 Travel time = 0.89 min. TC = 16.58 min.
 Adding area flow to street
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.826
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 RI index for soil (AMC 2) = 69.00
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Rainfall intensity = 3.043 (In/Hr) for a 100.0 year storm
 Subarea runoff = 1.382 (CFS) for 0.550 (Ac.)
 Total runoff = 9.162 (CFS) Total area = 3.400 (Ac.)
 Street flow at end of street = 9.162 (CFS)
 Half street flow at end of street = 4.581 (CFS)
 Depth of flow = 0.387 (Ft.), Average velocity = 2.507 (Ft/s)
 Flow width (from curb towards crown) = 13.040 (Ft.)

++++++
 Process from Point/Station 312.000 to Point/Station 314.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
 In Main Stream number: 2
 Stream flow area = 3.400 (Ac.)
 Runoff from this stream = 9.162 (CFS)
 Time of concentration = 16.58 min.
 Rainfall intensity = 3.043 (In/Hr)
 Program is now starting with Main Stream No. 3

 Process from Point/Station 313.000 to Point/Station 314.000
 **** INITIAL AREA EVALUATION ****

Initial area flow distance = 835.000(Ft.)
 Top (of initial area) elevation = 1456.100(Ft.)
 Bottom (of initial area) elevation = 1441.000(Ft.)
 Difference in elevation = 15.100(Ft.)
 Slope = 0.01808 s(percent)= 1.81
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 12.832 min.
 Rainfall intensity = 3.504(In/Hr) for a 100.0 year storm
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.834
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 RI index for soil(AMC 2) = 69.00
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Initial subarea runoff = 5.700(CFS)
 Total initial stream area = 1.950(Ac.)
 Pervious area fraction = 0.500

 Process from Point/Station 313.000 to Point/Station 314.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
 In Main Stream number: 3
 Stream flow area = 1.950(Ac.)
 Runoff from this stream = 5.700(CFS)
 Time of concentration = 12.83 min.
 Rainfall intensity = 3.504(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	21.505	15.39	3.170
2	9.162	16.58	3.043
3	5.700	12.83	3.504

Largest stream flow has longer or shorter time of concentration
 $Qp = 21.505 + \text{sum of}$
 $Qa \quad Tb/Ta$
 $9.162 * 0.928 = 8.502$
 $Qb \quad Ia/Ib$
 $5.700 * 0.905 = 5.158$
 $Qp = 35.165$

Total of 3 main streams to confluence:
 Flow rates before confluence point:
 21.505 9.162 5.700
 Area of streams before confluence:
 7.380 3.400 1.950

Results of confluence:
 Total flow rate = 35.165(CFS)
 Time of concentration = 15.390 min.
 Effective stream area after confluence = 12.730(Ac.)

 Process from Point/Station 314.000 to Point/Station 317.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1437.000(Ft.)

Downstream point/station elevation = 1433.000(Ft.)
Pipe length = 180.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 35.165(CFS)
Nearest computed pipe diameter = 24.00(In.)
Calculated individual pipe flow = 35.165(CFS)
Normal flow depth in pipe = 20.72(In.)
Flow top width inside pipe = 16.49(In.)
Critical depth could not be calculated.
Pipe flow velocity = 12.19(Ft/s)
Travel time through pipe = 0.25 min.
Time of concentration (TC) = 15.64 min.

Process from Point/Station 314.000 to Point/Station 317.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
Stream flow area = 12.730(Ac.)
Runoff from this stream = 35.165(CFS)
Time of concentration = 15.64 min.
Rainfall intensity = 3.143(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 315.000 to Point/Station 316.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 111.000(Ft.)
Top (of initial area) elevation = 1442.300(Ft.)
Bottom (of initial area) elevation = 1441.000(Ft.)
Difference in elevation = 1.300(Ft.)
Slope = 0.01171 s(percent) = 1.17
TC = $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 6.244 min.
Rainfall intensity = 5.207(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.854
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 0.889(CFS)
Total initial stream area = 0.200(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 316.000 to Point/Station 317.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1437.000(Ft.)
Downstream point/station elevation = 1433.000(Ft.)
Pipe length = 90.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.889(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.889(CFS)
Normal flow depth in pipe = 3.88(In.)
Flow top width inside pipe = 5.73(In.)
Critical Depth = 5.51(In.)
Pipe flow velocity = 6.62(Ft/s)
Travel time through pipe = 0.23 min.
Time of concentration (TC) = 6.47 min.

Process from Point/Station 316.000 to Point/Station 317.000

**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Stream flow area = 0.200(Ac.)
 Runoff from this stream = 0.889(CFS)
 Time of concentration = 6.47 min.
 Rainfall intensity = 5.106(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
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1	35.165	15.64	3.143
2	0.889	6.47	5.106

Largest stream flow has longer time of concentration

Qp = 35.165 + sum of

$$Q_b \frac{I_a}{I_b}$$

$$0.889 * \frac{5.106}{3.143} = 0.547$$
 Qp = 35.712

Total of 2 main streams to confluence:

Flow rates before confluence point:
 35.165 0.889

Area of streams before confluence:
 12.730 0.200

Results of confluence:

Total flow rate = 35.712(CFS)
 Time of concentration = 15.636 min.
 Effective stream area after confluence = 12.930(Ac.)

 Process from Point/Station 317.000 to Point/Station 317.000
 **** SUBAREA FLOW ADDITION ****

USER INPUT of soil data for subarea

Runoff Coefficient = 0.770
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.590
 Decimal fraction soil group D = 0.410
 RI index for soil(AMC 2) = 71.50
 Pervious area fraction = 1.000; Impervious fraction = 0.000
 Time of concentration = 15.64 min.
 Rainfall intensity = 3.143(In/Hr) for a 100.0 year storm
 Subarea runoff = 2.637(CFS) for 1.090(Ac.)
 Total runoff = 38.349(CFS) Total area = 14.020(Ac.)
 End of computations, total study area = 14.02 (Ac.)
 The following figures may

be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.539
 Area averaged RI index number = 69.2

Item 5.d

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989 - 2005 Version 7.1
Rational Hydrology Study Date: 06/12/15 File: ARDPON100.out

TRACT MAP 36785
POST-PROJECT ON-SITE HYDROLOGY FOR AREA D
100-YEAR STORM EVENT
FILENAME: ARDPON100.RRV

***** Hydrology Study Control Information *****

English (in-lb) Units used in input data file

Program License Serial Number 6269

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2
2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.500(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.500(In/Hr)
Slope of intensity duration curve = 0.5500

Process from Point/Station 401.000 to Point/Station 402.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 620.000(Ft.)
Top (of initial area) elevation = 1448.100(Ft.)
Bottom (of initial area) elevation = 1438.200(Ft.)
Difference in elevation = 9.900(Ft.)
Slope = 0.01597 s(percent)= 1.60
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 11.678 min.
Rainfall intensity = 3.690(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.841
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.730
Decimal fraction soil group D = 0.270
RI index for soil(AMC 2) = 70.60
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 9.404(CFS)
Total initial stream area = 3.030(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 402.000 to Point/Station 404.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1435.000(Ft.)
Downstream point/station elevation = 1430.000(Ft.)
Pipe length = 244.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 9.404(CFS)
 Nearest computed pipe diameter = 18.00(In.)
 Calculated individual pipe flow = 9.404(CFS)
 Normal flow depth in pipe = 10.31(In.)
 Flow top width inside pipe = 17.81(In.)
 Critical Depth = 14.22(In.)
 Pipe flow velocity = 8.98(Ft/s)
 Travel time through pipe = 0.45 min.
 Time of concentration (TC) = 12.13 min.

 Process from Point/Station 402.000 to Point/Station 404.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
 Stream flow area = 3.030(Ac.)
 Runoff from this stream = 9.404(CFS)
 Time of concentration = 12.13 min.
 Rainfall intensity = 3.614(In/Hr)
 Program is now starting with Main Stream No. 2

 Process from Point/Station 403.000 to Point/Station 404.000
 **** INITIAL AREA EVALUATION ****

Initial area flow distance = 581.000(Ft.)
 Top (of initial area) elevation = 1443.000(Ft.)
 Bottom (of initial area) elevation = 1433.900(Ft.)
 Difference in elevation = 9.100(Ft.)
 Slope = 0.01566 s(percent) = 1.57
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 11.423 min.
 Rainfall intensity = 3.735(In/Hr) for a 100.0 year storm
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.843
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.640
 Decimal fraction soil group D = 0.360
 RI index for soil(AMC 2) = 71.10
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Initial subarea runoff = 8.533(CFS)
 Total initial stream area = 2.710(Ac.)
 Pervious area fraction = 0.500

 Process from Point/Station 403.000 to Point/Station 404.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Stream flow area = 2.710(Ac.)
 Runoff from this stream = 8.533(CFS)
 Time of concentration = 11.42 min.
 Rainfall intensity = 3.735(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	9.404	12.13	3.614
2	8.533	11.42	3.735

Largest stream flow has longer time of concentration

Qp = 9.404 + sum of
 Qb Ia/Ib
 8.533 * 0.967 = 8.255

Qp = 17.659

Total of 2 main streams to confluence:

Flow rates before confluence point:

9.404 8.533

Area of streams before confluence:

3.030 2.710

Results of confluence:

Total flow rate = 17.659(CFS)

Time of concentration = 12.131 min.

Effective stream area after confluence = 5.740(Ac.)

Process from Point/Station 404.000 to Point/Station 406.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1430.000(Ft.)
Downstream point/station elevation = 1427.500(Ft.)
Pipe length = 244.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 17.659(CFS)
Nearest computed pipe diameter = 24.00(In.)
Calculated individual pipe flow = 17.659(CFS)
Normal flow depth in pipe = 15.82(In.)
Flow top width inside pipe = 22.75(In.)
Critical Depth = 18.17(In.)
Pipe flow velocity = 8.04(Ft/s)
Travel time through pipe = 0.51 min.
Time of concentration (TC) = 12.64 min.

Process from Point/Station 404.000 to Point/Station 406.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1

Stream flow area = 5.740(Ac.)

Runoff from this stream = 17.659(CFS)

Time of concentration = 12.64 min.

Rainfall intensity = 3.533(In/Hr)

Program is now starting with Main Stream No. 2

Process from Point/Station 405.000 to Point/Station 406.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 533.000(Ft.)
Top (of initial area) elevation = 1437.600(Ft.)
Bottom (of initial area) elevation = 1430.000(Ft.)
Difference in elevation = 7.600(Ft.)
Slope = 0.01426 s(percent) = 1.43
TC = $k(0.390)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$
Initial area time of concentration = 11.244 min.
Rainfall intensity = 3.768(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.839
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.960
Decimal fraction soil group D = 0.040
RI index for soil(AMC 2) = 69.20
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 7.079(CFS)
Total initial stream area = 2.240(Ac.)
Pervious area fraction = 0.500

 Process from Point/Station 405.000 to Point/Station 406.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Stream flow area = 2.240(Ac.)
 Runoff from this stream = 7.079(CFS)
 Time of concentration = 11.24 min.
 Rainfall intensity = 3.768(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	17.659	12.64	3.533
2	7.079	11.24	3.768

Largest stream flow has longer time of concentration

Qp = 17.659 + sum of
 Qb Ia/Ib
 7.079 * 0.938 = 6.638

Qp = 24.298

Total of 2 main streams to confluence:

Flow rates before confluence point:

17.659 7.079

Area of streams before confluence:

5.740 2.240

Results of confluence:

Total flow rate = 24.298(CFS)

Time of concentration = 12.637 min.

Effective stream area after confluence = 7.980(Ac.)

 Process from Point/Station 406.000 to Point/Station 408.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1427.500(Ft.)
 Downstream point/station elevation = 1425.000(Ft.)
 Pipe length = 81.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 24.298(CFS)
 Nearest computed pipe diameter = 21.00(In.)
 Calculated individual pipe flow = 24.298(CFS)
 Normal flow depth in pipe = 15.19(In.)
 Flow top width inside pipe = 18.79(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 13.04(Ft/s)
 Travel time through pipe = 0.10 min.
 Time of concentration (TC) = 12.74 min.

 Process from Point/Station 406.000 to Point/Station 408.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
 Stream flow area = 7.980(Ac.)
 Runoff from this stream = 24.298(CFS)
 Time of concentration = 12.74 min.
 Rainfall intensity = 3.517(In/Hr)
 Program is now starting with Main Stream No. 2

 Process from Point/Station 407.000 to Point/Station 408.000
 **** INITIAL AREA EVALUATION ****

Initial area flow distance = 188.000(Ft.)
 Top (of initial area) elevation = 1431.800(Ft.)
 Bottom (of initial area) elevation = 1429.000(Ft.)
 Difference in elevation = 2.800(Ft.)
 Slope = 0.01489 s(percent)= 1.49
 $TC = k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 7.347 min.
 Rainfall intensity = 4.761(In/Hr) for a 100.0 year storm
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.850
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 RI index for soil(AMC 2) = 69.00
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Initial subarea runoff = 2.589(CFS)
 Total initial stream area = 0.640(Ac.)
 Pervious area fraction = 0.500

 Process from Point/Station 407.000 to Point/Station 408.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Stream flow area = 0.640(Ac.)
 Runoff from this stream = 2.589(CFS)
 Time of concentration = 7.35 min.
 Rainfall intensity = 4.761(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	24.298	12.74	3.517
2	2.589	7.35	4.761

Largest stream flow has longer time of concentration

Qp = 24.298 + sum of
 $Q_b \quad I_a/I_b$
 $2.589 * 0.739 = 1.913$
 Qp = 26.211

Total of 2 main streams to confluence:

Flow rates before confluence point:
 24.298 2.589

Area of streams before confluence:
 7.980 0.640

Results of confluence:

Total flow rate = 26.211(CFS)
 Time of concentration = 12.740 min.
 Effective stream area after confluence = 8.620(Ac.)

 Process from Point/Station 408.000 to Point/Station 409.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1425.000(Ft.)
 Downstream point/station elevation = 1422.000(Ft.)
 Pipe length = 45.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 26.211(CFS)
 Nearest computed pipe diameter = 18.00(In.)
 Calculated individual pipe flow = 26.211(CFS)
 Normal flow depth in pipe = 14.25(In.)
 Flow top width inside pipe = 14.62(In.)

Critical depth could not be calculated.
Pipe flow velocity = 17.49(Ft/s)
Travel time through pipe = 0.04 min.
Time of concentration (TC) = 12.78 min.

Process from Point/Station 409.000 to Point/Station 409.000
**** SUBAREA FLOW ADDITION ****

USER INPUT of soil data for subarea

Runoff Coefficient = 0.794
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.190
Decimal fraction soil group D = 0.810
RI index for soil(AMC 2) = 73.90
Pervious area fraction = 1.000; Impervious fraction = 0.000
Time of concentration = 12.78 min.
Rainfall intensity = 3.511(In/Hr) for a 100.0 year storm
Subarea runoff = 2.062(CFS) for 0.740(Ac.)
Total runoff = 28.272(CFS) Total area = 9.360(Ac.)
End of computations, total study area = 9.36 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.540
Area averaged RI index number = 70.6

F
ON SITE

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989 - 2005 Version 7.1
Rational Hydrology Study Date: 06/12/15 File:ARFPON100.out

TRACT MAP 36785
POST-PROJECT ON-SITE HYDROLOGY FOR AREA F
100-YEAR STORM EVENT
FILENAME: ARFPON100.RRV

***** Hydrology Study Control Information *****

English (in-lb) Units used in input data file

Program License Serial Number 6269

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.500(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.500(In/Hr)
Slope of intensity duration curve = 0.5500

Process from Point/Station 601.000 to Point/Station 602.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 401.000(Ft.)
Top (of initial area) elevation = 1445.000(Ft.)
Bottom (of initial area) elevation = 1430.000(Ft.)
Difference in elevation = 15.000(Ft.)
Slope = 0.03741 s(percent)= 3.74
TC = k(0.417)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 8.847 min.
Rainfall intensity = 4.299(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.841
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.640
Decimal fraction soil group D = 0.360
RI index for soil(AMC 2) = 71.10
Pervious area fraction = 0.590; Impervious fraction = 0.410
Initial subarea runoff = 12.791(CFS)
Total initial stream area = 3.540(Ac.)
Pervious area fraction = 0.590
End of computations, total study area = 3.54 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.590
Area averaged RI index number = 71.1

E
Item S.e.

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989 - 2005 Version 7.1
Rational Hydrology Study Date: 06/12/15 File:AREPON100.out

TRACT MAP 36785
POST-PROJECT ON-SITE HYDROLOGY FOR AREA E
100-YEAR STORM EVENT
FILENAME: AREPON100.RRV

***** Hydrology Study Control Information *****

English (in-lb) Units used in input data file

Program License Serial Number 6269

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.500(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.500(In/Hr)
Slope of intensity duration curve = 0.5500

Process from Point/Station 501.000 to Point/Station 502.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 708.000(Ft.)
Top (of initial area) elevation = 1446.700(Ft.)
Bottom (of initial area) elevation = 1438.500(Ft.)
Difference in elevation = 8.200(Ft.)
Slope = 0.01158 s(percent)= 1.16
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 13.132 min.
Rainfall intensity = 3.459(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.834
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 11.160(CFS)
Total initial stream area = 3.870(Ac.) ✓
Pervious area fraction = 0.500

Process from Point/Station 502.000 to Point/Station 505.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1435.000(Ft.)
Downstream point/station elevation = 1432.000(Ft.)
Pipe length = 265.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 11.160(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 11.160(CFS)
Normal flow depth in pipe = 14.72(In.)
Flow top width inside pipe = 13.90(In.)
Critical Depth = 15.33(In.)
Pipe flow velocity = 7.21(Ft/s)
Travel time through pipe = 0.61 min.
Time of concentration (TC) = 13.74 min.

Process from Point/Station 502.000 to Point/Station 505.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
Stream flow area = 3.870(Ac.)
Runoff from this stream = 11.160(CFS)
Time of concentration = 13.74 min.
Rainfall intensity = 3.374(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 503.000 to Point/Station 504.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 443.000(Ft.)
Top (of initial area) elevation = 1447.800(Ft.)
Bottom (of initial area) elevation = 1434.700(Ft.)
Difference in elevation = 13.100(Ft.)
Slope = 0.02957 s(percent) = 2.96
TC = $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 9.025 min.
Rainfall intensity = 4.252(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.844
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 6.247(CFS)
Total initial stream area = 1.740(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 504.000 to Point/Station 505.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1437.400(Ft.)
End of street segment elevation = 1434.700(Ft.)
Length of street segment = 196.000(Ft.)
Height of curb above gutter flowline = 6.0(In.)
Width of half street (curb to crown) = 18.000(Ft.)
Distance from crown to crossfall grade break = 16.000(Ft.)
Slope from gutter to grade break (v/hz) = 0.020
Slope from grade break to crown (v/hz) = 0.020
Street flow is on [2] side(s) of the street
Distance from curb to property line = 10.000(Ft.)
Slope from curb to property line (v/hz) = 0.020
Gutter width = 2.000(Ft.)
Gutter hike from flowline = 2.000(In.)
Manning's N in gutter = 0.0150
Manning's N from gutter to grade break = 0.0150
Manning's N from grade break to crown = 0.0150
Estimated mean flow rate at midpoint of street = 8.069(CFS)
Depth of flow = 0.354(Ft.), Average velocity = 2.844(Ft/s)

Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 11.367(Ft.)
 Flow velocity = 2.84(Ft/s)
 Travel time = 1.15 min. TC = 10.17 min.
 Adding area flow to street
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.841
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 RI index for soil(AMC 2) = 69.00
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Rainfall intensity = 3.981(In/Hr) for a 100.0 year storm
 Subarea runoff = 3.516(CFS) for 1.050(Ac.)
 Total runoff = 9.763(CFS) Total area = 2.790(Ac.)
 Street flow at end of street = 9.763(CFS)
 Half street flow at end of street = 4.881(CFS)
 Depth of flow = 0.373(Ft.), Average velocity = 2.974(Ft/s)
 Flow width (from curb towards crown)= 12.307(Ft.)

 Process from Point/Station 504.000 to Point/Station 505.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Stream flow area = 2.790(Ac.)
 Runoff from this stream = 9.763(CFS)
 Time of concentration = 10.17 min.
 Rainfall intensity = 3.981(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	11.160	13.74	3.374
2	9.763	10.17	3.981

Largest stream flow has longer time of concentration
 $Q_p = 11.160 + \text{sum of } Q_b \cdot I_a/I_b$
 $Q_p = 19.434$

Total of 2 main streams to confluence:
 Flow rates before confluence point:
 11.160 9.763
 Area of streams before confluence:
 3.870 2.790

Results of confluence:
 Total flow rate = 19.434(CFS)
 Time of concentration = 13.744 min.
 Effective stream area after confluence = 6.660(Ac.)

 Process from Point/Station 505.000 to Point/Station 512.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1432.000(Ft.)
 Downstream point/station elevation = 1424.000(Ft.)
 Pipe length = 333.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 19.434(CFS)
 Nearest computed pipe diameter = 21.00(In.)
 Calculated individual pipe flow = 19.434(CFS)
 Normal flow depth in pipe = 14.09(In.)
 Flow top width inside pipe = 19.74(In.)

Critical Depth = 19.01(In.)
Pipe flow velocity = 11.32(Ft/s)
Travel time through pipe = 0.49 min.
Time of concentration (TC) = 14.23 min.

++++
Process from Point/Station 505.000 to Point/Station 512.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area = 6.660(Ac.)
Runoff from this stream = 19.434(CFS)
Time of concentration = 14.23 min.
Rainfall intensity = 3.309(In/Hr)
Program is now starting with Main Stream No. 2

++++
Process from Point/Station 506.000 to Point/Station 508.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 855.000(Ft.)
Top (of initial area) elevation = 1445.700(Ft.)
Bottom (of initial area) elevation = 1429.800(Ft.)
Difference in elevation = 15.900(Ft.)
Slope = 0.01860 s(percent)= 1.86
TC = $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 12.881 min.
Rainfall intensity = 3.496(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.839
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.680
Decimal fraction soil group D = 0.320
RI index for soil(AMC 2) = 70.90
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 6.894(CFS)
Total initial stream area = 2.350(Ac.)
Pervious area fraction = 0.500

++++
Process from Point/Station 506.000 to Point/Station 508.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
Stream flow area = 2.350(Ac.)
Runoff from this stream = 6.894(CFS)
Time of concentration = 12.88 min.
Rainfall intensity = 3.496(In/Hr)

++++
Process from Point/Station 507.000 to Point/Station 508.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 787.000(Ft.)
Top (of initial area) elevation = 1444.900(Ft.)
Bottom (of initial area) elevation = 1429.800(Ft.)
Difference in elevation = 15.100(Ft.)
Slope = 0.01919 s(percent)= 1.92
TC = $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 12.384 min.
Rainfall intensity = 3.573(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.849
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000

Decimal fraction soil group C = 0.080
 Decimal fraction soil group D = 0.920
 RI index for soil(AMC 2) = 74.50
 Pervious area fraction = 0.500; Impervious fraction = 0.500
 Initial subarea runoff = 12.771(CFS)
 Total initial stream area = 4.210(Ac.)
 Pervious area fraction = 0.500

 Process from Point/Station 507.000 to Point/Station 508.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
 Stream flow area = 4.210(Ac.)
 Runoff from this stream = 12.771(CFS)
 Time of concentration = 12.38 min.
 Rainfall intensity = 3.573(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	6.894	12.88	3.496
2	12.771	12.38	3.573

Largest stream flow has longer or shorter time of concentration

Qp = 12.771 + sum of
 Qa Tb/Ta
 6.894 * 0.961 = 6.628
 Qp = 19.398

Total of 2 streams to confluence:
 Flow rates before confluence point:
 6.894 12.771

Area of streams before confluence:
 2.350 4.210

Results of confluence:
 Total flow rate = 19.398(CFS)
 Time of concentration = 12.384 min.
 Effective stream area after confluence = 6.560(Ac.)

 Process from Point/Station 508.000 to Point/Station 511.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1429.800(Ft.)
 End of street segment elevation = 1429.200(Ft.)
 Length of street segment = 57.000(Ft.)
 Height of curb above gutter flowline = 6.0(In.)
 Width of half street (curb to crown) = 18.000(Ft.)
 Distance from crown to crossfall grade break = 16.000(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on {2} side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 2.000(Ft.)
 Gutter hike from flowline = 2.000(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 19.650(CFS)
 Depth of flow = 0.471(Ft.), Average velocity = 3.176(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 17.223(Ft.)
 Flow velocity = 3.18(Ft/s)
 Travel time = 0.30 min. TC = 12.68 min.
 Adding area flow to street
 USER INPUT of soil data for subarea

Runoff Coefficient = 0.836
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.880
Decimal fraction soil group D = 0.120
RI index for soil(AMC 2) = 69.70
Pervious area fraction = 0.500; Impervious fraction = 0.500
Rainfall intensity = 3.526(In/Hr) for a 100.0 year storm
Subarea runoff = 0.501(CFS) for 0.170(Ac.)
Total runoff = 19.900(CFS) Total area = 6.730(Ac.)
Street flow at end of street = 19.900(CFS)
Half street flow at end of street = 9.950(CFS)
Depth of flow = 0.473(Ft.), Average velocity = 3.186(Ft/s)
Flow width (from curb towards crown)= 17.309(Ft.)

Process from Point/Station 508.000 to Point/Station 511.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
Stream flow area = 6.730(Ac.)
Runoff from this stream = 19.900(CFS)
Time of concentration = 12.68 min.
Rainfall intensity = 3.526(In/Hr)

Process from Point/Station 509.000 to Point/Station 510.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 787.000(Ft.)
Top (of initial area) elevation = 1432.000(Ft.)
Bottom (of initial area) elevation = 1429.000(Ft.)
Difference in elevation = 3.000(Ft.)
Slope = 0.00381 s(percent)= 0.38
TC = $k(0.390)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 17.109 min.
Rainfall intensity = 2.991(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.825
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.990
Decimal fraction soil group D = 0.010
RI index for soil(AMC 2) = 69.10
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff = 1.900(CFS)
Total initial stream area = 0.770(Ac.)
Pervious area fraction = 0.500

Process from Point/Station 510.000 to Point/Station 511.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1426.000(Ft.)
Downstream point/station elevation = 1425.000(Ft.)
Pipe length = 180.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 1.900(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 1.900(CFS)
Normal flow depth in pipe = 7.51(In.)
Flow top width inside pipe = 11.61(In.)
Critical Depth = 7.05(In.)
Pipe flow velocity = 3.68(Ft/s)
Travel time through pipe = 0.82 min.
Time of concentration (TC) = 17.93 min.

Process from Point/Station 510.000 to Point/Station 511.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
 Stream flow area = 0.770(Ac.)
 Runoff from this stream = 1.900(CFS)
 Time of concentration = 17.93 min.
 Rainfall intensity = 2.915(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	19.900	12.69	3.526
2	1.900	17.93	2.915

Largest stream flow has longer or shorter time of concentration
 Qp = 19.900 + sum of
 Qa Tb/Ta
 1.900 * 0.708 = 1.345
 Qp = 21.244

Total of 2 streams to confluence:
 Flow rates before confluence point:
 19.900 1.900
 Area of streams before confluence:
 6.730 0.770

Results of confluence:
 Total flow rate = 21.244(CFS)
 Time of concentration = 12.683 min.
 Effective stream area after confluence = 7.500(Ac.)

 Process from Point/Station 511.000 to Point/Station 512.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1425.000(Ft.)
 Downstream point/station elevation = 1424.000(Ft.)
 Pipe length = 60.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 21.244(CFS)
 Nearest computed pipe diameter = 24.00(In.)
 Calculated individual pipe flow = 21.244(CFS)
 Normal flow depth in pipe = 15.19(In.)
 Flow top width inside pipe = 23.14(In.)
 Critical Depth = 19.80(In.)
 Pipe flow velocity = 10.14(Ft/s)
 Travel time through pipe = 0.10 min.
 Time of concentration (TC) = 12.78 min.

 Process from Point/Station 511.000 to Point/Station 512.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
 In Main Stream number: 2
 Stream flow area = 7.500(Ac.)
 Runoff from this stream = 21.244(CFS)
 Time of concentration = 12.78 min.
 Rainfall intensity = 3.511(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	19.434	14.23	3.309
2	21.244	12.78	3.511

Largest stream flow has longer or shorter time of concentration
 Qp = 21.244 + sum of

Qa Tb/Ta
 19.434 * 0.898 = 17.450
 Qp = 38.694

Total of 2 main streams to confluence:
 Flow rates before confluence point:
 19.434 21.244
 Area of streams before confluence:
 6.660 7.500

Results of confluence:
 Total flow rate = 38.694 (CFS)
 Time of concentration = 12.782 min.
 Effective stream area after confluence = 14.160 (Ac.)

++++++
 Process from Point/Station 512.000 to Point/Station 513.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1424.000 (Ft.)
 Downstream point/station elevation = 1422.000 (Ft.)
 Pipe length = 52.00 (Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 38.694 (CFS)
 Nearest computed pipe diameter = 24.00 (In.)
 Calculated individual pipe flow = 38.694 (CFS)
 Normal flow depth in pipe = 17.34 (In.)
 Flow top width inside pipe = 21.49 (In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 15.91 (Ft/s)
 Travel time through pipe = 0.05 min.
 Time of concentration (TC) = 12.84 min.

++++++
 Process from Point/Station 513.000 to Point/Station 513.000
 **** SUBAREA FLOW ADDITION ****

USER INPUT of soil data for subarea
 Runoff Coefficient = 0.791
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.250
 Decimal fraction soil group D = 0.750
 RI index for soil (AMC 2) = 73.50
 Pervious area fraction = 1.000; Impervious fraction = 0.000
 Time of concentration = 12.84 min.
 Rainfall intensity = 3.503 (In/Hr) for a 100.0 year storm
 Subarea runoff = 4.186 (CFS) for 1.510 (Ac.)
 Total runoff = 42.881 (CFS) Total area = 15.670 (Ac.)
 End of computations, total study area = 15.67 (Ac.)
 The following figures may
 be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction (Ap) = 0.548
 Area averaged RI index number = 71.2

F
On site
Item 5. f.

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989 - 2005 Version 7.1
Rational Hydrology Study Date: 07/24/14 File:ARFEX100.out

100-YEAR RATIONAL METHOD FOR AREA F
PRE-PROJECT CONDITION
FN: ARFEX100.RRV

***** Hydrology Study Control Information *****

English (in-lb) Units used in input data file

Program License Serial Number 6269

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.200(In/Hr)
Slope of intensity duration curve = 0.5500

Process from Point/Station 601.000 to Point/Station 602.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 583.000(Ft.)
Top (of initial area) elevation = 1644.000(Ft.)
Bottom (of initial area) elevation = 1496.000(Ft.)
Difference in elevation = 148.000(Ft.)
Slope = 0.25386 s(percent) = 25.39
TC = $k(-1.036)*[(length^3)/(elevation\ change)]^{0.2}$
Warning: TC computed to be less than 5 min.; program is assuming the
time of concentration is 5 minutes.
Initial area time of concentration = 5.000 min.
Rainfall intensity = 4.707(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.868
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
RI index for soil(AMC 2) = 88.00
Pervious area fraction = 0.970; Impervious fraction = 0.030
Initial subarea runoff = 7.758(CFS)
Total initial stream area = 1.900(Ac.)
Pervious area fraction = 0.970

Process from Point/Station 602.000 to Point/Station 603.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1496.000(Ft.)

End of natural channel elevation = 1450.000(Ft.)
Length of natural channel = 1297.000(Ft.)
Estimated mean flow rate at midpoint of channel = 42.058(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
Velocity(ft/s) = $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{.5}))$
Velocity using mean channel flow = 6.94(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
Normal channel slope = 0.0355
Corrected/adjusted channel slope = 0.0355
Travel time = 3.12 min. TC = 8.12 min.

Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.846
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.700
Decimal fraction soil group D = 0.300
RI index for soil(AMC 2) = 85.00
Pervious area fraction = 0.980; Impervious fraction = 0.020
Rainfall intensity = 3.606(In/Hr) for a 100.0 year storm
Subarea runoff = 51.248(CFS) for 16.800(Ac.)
Total runoff = 59.007(CFS) Total area = 18.700(Ac.)

Process from Point/Station 603.000 to Point/Station 607.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1450.000(Ft.)
End of natural channel elevation = 1444.000(Ft.)
Length of natural channel = 526.000(Ft.)
Estimated mean flow rate at midpoint of channel = 72.891(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
Velocity(ft/s) = $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{.5}))$
Velocity using mean channel flow = 4.61(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
Normal channel slope = 0.0114
Corrected/adjusted channel slope = 0.0114
Travel time = 1.90 min. TC = 10.02 min.

Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.834
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 84.00
Pervious area fraction = 1.000; Impervious fraction = 0.000
Rainfall intensity = 3.212(In/Hr) for a 100.0 year storm
Subarea runoff = 23.575(CFS) for 8.800(Ac.)
Total runoff = 82.582(CFS) Total area = 27.500(Ac.)

Process from Point/Station 603.000 to Point/Station 607.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 27.500(Ac.)

Runoff from this stream = 82.582(CFS)
Time of concentration = 10.02 min.
Rainfall intensity = 3.212(In/Hr)

Process from Point/Station 604.000 to Point/Station 605.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 910.000(Ft.)
Top (of initial area) elevation = 1572.000(Ft.)
Bottom (of initial area) elevation = 1462.000(Ft.)
Difference in elevation = 110.000(Ft.)
Slope = 0.12088 s(percent)= 12.09
TC = $k(-0.964)*[(length^3)/(elevation\ change)]^{0.2}$
Warning: TC computed to be less than 5 min.; program is assuming the
time of concentration is 5 minutes.
Initial area time of concentration = 5.000 min.
Rainfall intensity = 4.707(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.860
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.700
Decimal fraction soil group D = 0.300
RI index for soil(AMC 2) = 85.10
Pervious area fraction = 0.930; Impervious fraction = 0.070
Initial subarea runoff = 11.745(CFS)
Total initial stream area = 2.900(Ac.)
Pervious area fraction = 0.930

Process from Point/Station 605.000 to Point/Station 606.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1462.000(Ft.)
End of natural channel elevation = 1451.000(Ft.)
Length of natural channel = 620.000(Ft.)
Estimated mean flow rate at midpoint of channel = 18.630(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
Velocity(ft/s) = $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{0.5}))$
Velocity using mean channel flow = 3.92(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
Normal channel slope = 0.0177
Corrected/adjusted channel slope = 0.0177
Travel time = 2.64 min. TC = 7.64 min.

Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.843
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 84.00
Pervious area fraction = 1.000; Impervious fraction = 0.000
Rainfall intensity = 3.728(In/Hr) for a 100.0 year storm
Subarea runoff = 10.681(CFS) for 3.400(Ac.)
Total runoff = 22.426(CFS) Total area = 6.300(Ac.)

Process from Point/Station 606.000 to Point/Station 607.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1451.000(Ft.)
 End of natural channel elevation = 1444.000(Ft.)
 Length of natural channel = 719.000(Ft.)
 Estimated mean flow rate at midpoint of channel = 38.444(CFS)

Natural valley channel type used
 L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{.5}))$
 Velocity using mean channel flow = 3.54(Ft/s)

Correction to map slope used on extremely rugged channels with
 drops and waterfalls (Plate D-6.2)
 Normal channel slope = 0.0097
 Corrected/adjusted channel slope = 0.0097
 Travel time = 3.38 min. TC = 11.02 min.

Adding area flow to channel
 USER INPUT of soil data for subarea
 Runoff Coefficient = 0.834
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.900
 Decimal fraction soil group D = 0.100
 RI index for soil(AMC 2) = 84.60
 Pervious area fraction = 1.000; Impervious fraction = 0.000
 Rainfall intensity = 3.047(In/Hr) for a 100.0 year storm
 Subarea runoff = 22.863(CFS) for 9.000(Ac.)
 Total runoff = 45.289(CFS) Total area = 15.300(Ac.)

 Process from Point/Station 606.000 to Point/Station 607.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 15.300(Ac.)
 Runoff from this stream = 45.289(CFS)
 Time of concentration = 11.02 min.
 Rainfall intensity = 3.047(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
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1	82.582	10.02	3.212
2	45.289	11.02	3.047

Largest stream flow has longer or shorter time of concentration
 $Q_p = 82.582 + \text{sum of } \frac{Q_a \cdot T_b/T_a}{45.289 * 0.909} = 41.158$
 $Q_p = 123.740$

Total of 2 streams to confluence:
 Flow rates before confluence point:
 82.582 45.289
 Area of streams before confluence:
 27.500 15.300
 Results of confluence:
 Total flow rate = 123.740(CFS)
 Time of concentration = 10.016 min.
 Effective stream area after confluence = 42.800(Ac.)

 Process from Point/Station 607.000 to Point/Station 608.000
 **** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1444.000(Ft.)
 End of natural channel elevation = 1418.000(Ft.)

Length of natural channel = 2066.000(Ft.)
Estimated mean flow rate at midpoint of channel = 195.150(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
Velocity(ft/s) = $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{0.5}))$
Velocity using mean channel flow = 6.53(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
Normal channel slope = 0.0126
Corrected/adjusted channel slope = 0.0126
Travel time = 5.27 min. TC = 15.29 min.

Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.823
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.200
RI index for soil(AMC 2) = 84.80
Pervious area fraction = 1.000; Impervious fraction = 0.000
Rainfall intensity = 2.545(In/Hr) for a 100.0 year storm
Subarea runoff = 103.451(CFS) for 49.400(Ac.)
Total runoff = 227.191(CFS) Total area = 92.200(Ac.)

Process from Point/Station 608.000 to Point/Station 609.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1418.000(Ft.)
End of natural channel elevation = 1416.000(Ft.)
Length of natural channel = 730.000(Ft.)
Estimated mean flow rate at midpoint of channel = 246.534(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
Velocity(ft/s) = $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{0.5}))$
Velocity using mean channel flow = 3.28(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
Normal channel slope = 0.0027
Corrected/adjusted channel slope = 0.0027
Travel time = 3.71 min. TC = 19.00 min.

Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.822
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.500
Decimal fraction soil group D = 0.500
RI index for soil(AMC 2) = 86.10
Pervious area fraction = 1.000; Impervious fraction = 0.000
Rainfall intensity = 2.258(In/Hr) for a 100.0 year storm
Subarea runoff = 29.135(CFS) for 15.700(Ac.)
Total runoff = 256.326(CFS) Total area = 107.900(Ac.)
End of computations, total study area = 107.90 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.994
Area averaged RI index number = 85.0

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Item 5.g.

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989 - 2005 Version 7.1
Rational Hydrology Study Date: 06/16/15 File:ARFPOST100.out

TRACT 36785
100-YEAR RATIONAL METHOD FOR AREA F
OFFSITE POST PROJECT CONDITION
FN: ARFPOST100.PRV

***** Hydrology Study Control Information *****

English (in-lb) Units used in input data file

Program License Serial Number 6269

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.500(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.500(In/Hr)
Slope of intensity duration curve = 0.5500

Process from Point/Station 601.000 to Point/Station 602.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 606.000(Ft.)
Top (of initial area) elevation = 1648.000(Ft.)
Bottom (of initial area) elevation = 1496.000(Ft.)
Difference in elevation = 152.000(Ft.)
Slope = 0.25083 s(percent) = 25.08
TC = $k(0.530)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$
Initial area time of concentration = 9.065 min.
Rainfall intensity = 4.241(In/Hr) for a 100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.866
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
RI index for soil(AMC 2) = 89.00
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff = 6.982(CFS)
Total initial stream area = 1.900(Ac.)
Pervious area fraction = 1.000

Process from Point/Station 602.000 to Point/Station 605.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1496.000(Ft.)
End of natural channel elevation = 1475.000(Ft.)
Length of natural channel = 337.000(Ft.)

Estimated mean flow rate at midpoint of channel = 14.882(CFS)

Natural valley channel type used

L.A. County flood control formula for channel velocity:

Velocity(ft/s) = $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{0.5}))$

Velocity using mean channel flow = 6.91(Ft/s)

Correction to map slope used on extremely rugged channels with drops and waterfalls (Plate D-6.2)

Normal channel slope = 0.0623

Corrected/adjusted channel slope = 0.0623

Travel time = 0.81 min. TC = 9.88 min.

Adding area flow to channel

UNDEVELOPED (poor cover) subarea

Runoff Coefficient = 0.865

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 0.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 1.000

RI index for soil(AMC 2) = 89.00

Pervious area fraction = 1.000; Impervious fraction = 0.000

Rainfall intensity = 4.046(In/Hr) for a 100.0 year storm

Subarea runoff = 15.045(CFS) for 4.300(Ac.)

Total runoff = 22.026(CFS) Total area = 6.200(Ac.)

Process from Point/Station 602.000 to Point/Station 605.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1

Stream flow area = 6.200(Ac.)

Runoff from this stream = 22.026(CFS)

Time of concentration = 9.88 min.

Rainfall intensity = 4.046(In/Hr)

Program is now starting with Main Stream No. 2

Process from Point/Station 603.000 to Point/Station 604.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 527.000(Ft.)

Top (of initial area) elevation = 1485.000(Ft.)

Bottom (of initial area) elevation = 1472.000(Ft.)

Difference in elevation = 13.000(Ft.)

Slope = 0.02467 s(percent) = 2.47

TC = $k(0.530)*[(\text{length}^3)/(\text{elevation change})]^{0.2}$

Initial area time of concentration = 13.632 min.

Rainfall intensity = 3.389(In/Hr) for a 100.0 year storm

UNDEVELOPED (poor cover) subarea

Runoff Coefficient = 0.846

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 0.000

Decimal fraction soil group C = 1.000

Decimal fraction soil group D = 0.000

RI index for soil(AMC 2) = 86.00

Pervious area fraction = 1.000; Impervious fraction = 0.000

Initial subarea runoff = 2.866(CFS)

Total initial stream area = 1.000(Ac.)

Pervious area fraction = 1.000

Process from Point/Station 604.000 to Point/Station 605.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1472.000(Ft.)

Downstream point/station elevation = 1469.000(Ft.)
 Pipe length = 492.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 2.866(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 2.866(CFS)
 Normal flow depth in pipe = 8.10(In.)
 Flow top width inside pipe = 14.95(In.)
 Critical Depth = 8.17(In.)
 Pipe flow velocity = 4.24(Ft/s)
 Travel time through pipe = 1.93 min.
 Time of concentration (TC) = 15.57 min.

 Process from Point/Station 604.000 to Point/Station 605.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Stream flow area = 1.000(Ac.)
 Runoff from this stream = 2.866(CFS)
 Time of concentration = 15.57 min.
 Rainfall intensity = 3.151(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	22.026	9.88	4.046
2	2.866	15.57	3.151

Largest stream flow has longer or shorter time of concentration

Qp = 22.026 + sum of

$$Q_a \quad T_b/T_a$$

$$2.866 * 0.635 = 1.819$$
 Qp = 23.845

Total of 2 main streams to confluence:
 Flow rates before confluence point:
 22.026 2.866
 Area of streams before confluence:
 6.200 1.000

Results of confluence:
 Total flow rate = 23.845(CFS)
 Time of concentration = 9.878 min.
 Effective stream area after confluence = 7.200(Ac.)

 Process from Point/Station 605.000 to Point/Station 608.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1469.000(Ft.)
 Downstream point/station elevation = 1467.000(Ft.)
 Pipe length = 400.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 23.845(CFS)
 Nearest computed pipe diameter = 30.00(In.)
 Calculated individual pipe flow = 23.845(CFS)
 Normal flow depth in pipe = 20.72(In.)
 Flow top width inside pipe = 27.73(In.)
 Critical Depth = 19.95(In.)
 Pipe flow velocity = 6.60(Ft/s)
 Travel time through pipe = 1.01 min.
 Time of concentration (TC) = 10.89 min.

 Process from Point/Station 605.000 to Point/Station 608.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
 In Main Stream number: 1
 Stream flow area = 7.200(Ac.)
 Runoff from this stream = 23.845(CFS)
 Time of concentration = 10.89 min.
 Rainfall intensity = 3.835(In/Hr)
 Program is now starting with Main Stream No. 2

 Process from Point/Station 606.000 to Point/Station 607.000
 **** INITIAL AREA EVALUATION ****

Initial area flow distance = 642.000(Ft.)
 Top (of initial area) elevation = 1580.000(Ft.)
 Bottom (of initial area) elevation = 1469.300(Ft.)
 Difference in elevation = 110.700(Ft.)
 Slope = 0.17243 s(percent)= 17.24
 $TC = k(0.530)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 9.999 min.
 Rainfall intensity = 4.019(In/Hr) for a 100.0 year storm
 UNDEVELOPED (poor cover) subarea
 Runoff Coefficient = 0.861
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.320
 Decimal fraction soil group D = 0.680
 RI index for soil(AMC 2) = 88.04
 Pervious area fraction = 1.000; Impervious fraction = 0.000
 Initial subarea runoff = 12.805(CFS)
 Total initial stream area = 3.700(Ac.)
 Pervious area fraction = 1.000

 Process from Point/Station 607.000 to Point/Station 608.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1469.300(Ft.)
 Downstream point/station elevation = 1467.000(Ft.)
 Pipe length = 137.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 12.805(CFS)
 Nearest computed pipe diameter = 18.00(In.)
 Calculated individual pipe flow = 12.805(CFS)
 Normal flow depth in pipe = 13.88(In.)
 Flow top width inside pipe = 15.13(In.)
 Critical Depth = 16.13(In.)
 Pipe flow velocity = 8.76(Ft/s)
 Travel time through pipe = 0.26 min.
 Time of concentration (TC) = 10.26 min.

 Process from Point/Station 607.000 to Point/Station 608.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
 In Main Stream number: 2
 Stream flow area = 3.700(Ac.)
 Runoff from this stream = 12.805(CFS)
 Time of concentration = 10.26 min.
 Rainfall intensity = 3.962(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	23.845	10.89	3.835
2	12.805	10.26	3.962

Largest stream flow has longer time of concentration
 $Q_p = 23.845 + \text{sum of}$
 $Q_b \quad I_a/I_b$
 $12.805 * 0.968 = 12.393$
 $Q_p = 36.238$

Total of 2 main streams to confluence:
Flow rates before confluence point:
23.845 12.805
Area of streams before confluence:
7.200 3.700

Results of confluence:
Total flow rate = 36.238(CFS)
Time of concentration = 10.889 min.
Effective stream area after confluence = 10.900(Ac.)

Process from Point/Station 608.000 to Point/Station 609.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1467.000(Ft.)
Downstream point/station elevation = 1415.500(Ft.)
Pipe length = 3907.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 36.238(CFS)
Nearest computed pipe diameter = 27.00(In.)
Calculated individual pipe flow = 36.238(CFS)
Normal flow depth in pipe = 22.64(In.)
Flow top width inside pipe = 19.87(In.)
Critical Depth = 24.41(In.)
Pipe flow velocity = 10.18(Ft/s)
Travel time through pipe = 6.39 min.
Time of concentration (TC) = 17.28 min.

Process from Point/Station 609.000 to Point/Station 609.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.842
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.750
Decimal fraction soil group D = 0.250
RI index for soil(AMC 2) = 86.75
Pervious area fraction = 1.000; Impervious fraction = 0.000
Time of concentration = 17.28 min.
Rainfall intensity = 2.974(In/Hr) for a 100.0 year storm
Subarea runoff = 27.308(CFS) for 10.900(Ac.)
Total runoff = 63.547(CFS) Total area = 21.800(Ac.)

Process from Point/Station 609.000 to Point/Station 610.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1415.500(Ft.)
Downstream point/station elevation = 1415.000(Ft.)
Pipe length = 52.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 63.547(CFS)
Nearest computed pipe diameter = 36.00(In.)
Calculated individual pipe flow = 63.547(CFS)
Normal flow depth in pipe = 28.64(In.)
Flow top width inside pipe = 29.04(In.)
Critical Depth = 30.74(In.)
Pipe flow velocity = 10.54(Ft/s)
Travel time through pipe = 0.08 min.
Time of concentration (TC) = 17.36 min.

Process from Point/Station 610.000 to Point/Station 611.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1415.000(Ft.)
End of natural channel elevation = 1414.000(Ft.)
Length of natural channel = 537.000(Ft.)
Estimated mean flow rate at midpoint of channel = 74.041(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
Velocity(ft/s) = $(7 + 8(q(\text{English Units})^{.352})(\text{slope}^{0.5}))$
Velocity using mean channel flow = 1.87(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
Normal channel slope = 0.0019
Corrected/adjusted channel slope = 0.0019
Travel time = 4.78 min. TC = 22.14 min.

Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.835
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.750
Decimal fraction soil group D = 0.250
RI index for soil(AMC 2) = 86.75
Pervious area fraction = 1.000; Impervious fraction = 0.000
Rainfall intensity = 2.595(In/Hr) for a 100.0 year storm
Subarea runoff = 15.594(CFS) for 7.200(Ac.)
Total runoff = 79.141(CFS) Total area = 29.000(Ac.)
End of computations, total study area = 29.00 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number = 87.4

Q
Ivan S. h.

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989 - 2005 Version 7.1
Rational Hydrology Study Date: 06/16/15 File:ARQPON100.out

TRACT MAP 36785
POST-PROJECT ON-SITE HYDROLOGY FOR AREA Q
100-YEAR STORM EVENT
FILENAME: ARQPON100.RRV

***** Hydrology Study Control Information *****

English (in-lb) Units used in input data file

Program License Serial Number 6269

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.500(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.500(In/Hr)
Slope of intensity duration curve = 0.5500

Process from Point/Station 1701.000 to Point/Station 1702.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 292.000(Ft.)
Top (of initial area) elevation = 1477.000(Ft.)
Bottom (of initial area) elevation = 1474.100(Ft.)
Difference in elevation = 2.900(Ft.)
Slope = 0.00993 s(percent) = 0.99
TC = $k(0.353)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 8.601 min.
Rainfall intensity = 4.366(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.867
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.300; Impervious fraction = 0.700
Initial subarea runoff = 2.840(CFS) ✓
Total initial stream area = 0.750(AC.)
Pervious area fraction = 0.300

Process from Point/Station 1702.000 to Point/Station 1703.000
**** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 1474.100(Ft.)
Downstream point elevation = 1470.200(Ft.)
Channel length thru subarea = 80.000(Ft.)

Channel base width = 5.000(Ft.)
Slope or 'Z' of left channel bank = 2.000
Slope or 'Z' of right channel bank = 2.000
Manning's 'N' = 0.025
Maximum depth of channel = 2.000(Ft.)
Flow(q) thru subarea = 2.840(CFS)
Depth of flow = 0.151(Ft.), Average velocity = 3.553(Ft/s)
Channel flow top width = 5.603(Ft.)
Flow Velocity = 3.55(Ft/s)
Travel time = 0.38 min.
Time of concentration = 8.98 min.

Sub-Channel No. 1 Critical depth = 0.209(Ft.)
' ' ' Critical flow top width = 5.836(Ft.)
' ' ' Critical flow velocity = 2.509(Ft/s)
' ' ' Critical flow area = 1.132(Sq.Ft)

Process from Point/Station 1703.000 to Point/Station 1706.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1470.200(Ft.)
Downstream point/station elevation = 1470.000(Ft.)
Pipe length = 466.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.840(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 2.840(CFS)
Normal flow depth in pipe = 15.09(In.)
Flow top width inside pipe = 18.88(In.)
Critical Depth = 7.33(In.)
Pipe flow velocity = 1.54(Ft/s)
Travel time through pipe = 5.06 min.
Time of concentration (TC) = 14.03 min.

Process from Point/Station 1703.000 to Point/Station 1706.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
Stream flow area = 0.750(Ac.)
Runoff from this stream = 2.840(CFS)
Time of concentration = 14.03 min.
Rainfall intensity = 3.336(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 1704.000 to Point/Station 1705.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 196.000(Ft.)
Top (of initial area) elevation = 1477.000(Ft.)
Bottom (of initial area) elevation = 1475.000(Ft.)
Difference in elevation = 2.000(Ft.)
Slope = 0.01020 s(percent) = 1.02
TC = $k(0.353) * [(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 7.293 min.
Rainfall intensity = 4.780(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.870
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 69.00
Pervious area fraction = 0.300; Impervious fraction = 0.700
Initial subarea runoff = 3.202(CFS)

Total initial stream area = 0.770(Ac.)
Pervious area fraction = 0.300

Process from Point/Station 1705.000 to Point/Station 1706.000
**** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 1475.000(Ft.)
Downstream point elevation = 1470.000(Ft.)
Channel length thru subarea = 93.000(Ft.)
Channel base width = 5.000(Ft.)
Slope or 'Z' of left channel bank = 2.000
Slope or 'Z' of right channel bank = 2.000
Manning's 'N' = 0.025
Maximum depth of channel = 2.000(Ft.)
Flow(q) thru subarea = 3.202(CFS)
Depth of flow = 0.157(Ft.), Average velocity = 3.831(Ft/s)
Channel flow top width = 5.629(Ft.)
Flow Velocity = 3.83(Ft/s)
Travel time = 0.40 min.
Time of concentration = 7.70 min.

Sub-Channel No. 1 Critical depth = 0.227(Ft.)
Critical flow top width = 5.906(Ft.)
Critical flow velocity = 2.592(Ft/s)
Critical flow area = 1.235(Sq.Ft)

Process from Point/Station 1705.000 to Point/Station 1706.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
Stream flow area = 0.770(Ac.)
Runoff from this stream = 3.202(CFS)
Time of concentration = 7.70 min.
Rainfall intensity = 4.641(In/Hr)
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	2.840	14.03	3.336
2	3.202	7.70	4.641

Largest stream flow has longer or shorter time of concentration

Qp = 3.202 + sum of
Qa Tb/Ta
2.840 * 0.549 = 1.558
Qp = 4.760

Total of 2 main streams to confluence:

Flow rates before confluence point:

2.840 3.202

Area of streams before confluence:

0.750 0.770

Results of confluence:

Total flow rate = 4.760(CFS)

Time of concentration = 7.698 min.

Effective stream area after confluence = 1.520(Ac.)

Process from Point/Station 1706.000 to Point/Station 1710.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1470.000(Ft.)
Downstream point/station elevation = 1467.000(Ft.)
Pipe length = 508.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 4.760(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 4.760(CFS)
Normal flow depth in pipe = 11.77(In.)
Flow top width inside pipe = 12.34(In.)
Critical Depth = 10.61(In.)
Pipe flow velocity = 4.61(Ft/s)
Travel time through pipe = 1.84 min.
Time of concentration (TC) = 9.54 min.

Process from Point/Station 1706.000 to Point/Station 1710.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area = 1.520(Ac.)
Runoff from this stream = 4.760(CFS)
Time of concentration = 9.54 min.
Rainfall intensity = 4.125(In/Hr)
Program is now starting with Main Stream No. 2

Process from Point/Station 1707.000 to Point/Station 1708.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 223.000(Ft.)
Top (of initial area) elevation = 1476.200(Ft.)
Bottom (of initial area) elevation = 1474.000(Ft.)
Difference in elevation = 2.200(Ft.)
Slope = 0.00987 s(percent) = 0.99
TC = $k(0.353) * \{(\text{length}^3) / (\text{elevation change})\}^{0.2}$
Initial area time of concentration = 7.732 min.
Rainfall intensity = 4.629(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.873
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.520
Decimal fraction soil group D = 0.480
RI index for soil(AMC 2) = 71.90
Pervious area fraction = 0.300; Impervious fraction = 0.700
Initial subarea runoff = 2.464(CFS)
Total initial stream area = 0.610(Ac.)
Pervious area fraction = 0.300

Process from Point/Station 1708.000 to Point/Station 1709.000
**** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 1474.000(Ft.)
Downstream point elevation = 1469.000(Ft.)
Channel length thru subarea = 25.000(Ft.)
Channel base width = 5.000(Ft.)
Slope or 'Z' of left channel bank = 2.000
Slope or 'Z' of right channel bank = 2.000
Manning's 'N' = 0.025
Maximum depth of channel = 2.000(Ft.)
Flow(q) thru subarea = 2.464(CFS)
Depth of flow = 0.091(Ft.) Average velocity = 5.227(Ft/s)
Channel flow top width = 5.364(Ft.)
Flow Velocity = 5.23(Ft/s)
Travel time = 0.08 min.
Time of concentration = 7.81 min.

Sub-Channel No. 1 Critical depth = 0.191(Ft.)
 Critical flow top width = 5.766(Ft.)
 Critical flow velocity = 2.392(Ft/s)
 Critical flow area = 1.030(Sq.Ft)

Process from Point/Station 1709.000 to Point/Station 1710.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1469.000(Ft.)
 Downstream point/station elevation = 1467.000(Ft.)
 Pipe length = 56.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 2.464(CFS)
 Nearest computed pipe diameter = 9.00(In.)
 Calculated individual pipe flow = 2.464(CFS)
 Normal flow depth in pipe = 6.02(In.)
 Flow top width inside pipe = 8.47(In.)
 Critical Depth = 8.28(In.)
 Pipe flow velocity = 7.84(Ft/s)
 Travel time through pipe = 0.12 min.
 Time of concentration (TC) = 7.93 min.

Process from Point/Station 1709.000 to Point/Station 1710.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Stream flow area = 0.610(Ac.)
 Runoff from this stream = 2.464(CFS)
 Time of concentration = 7.93 min.
 Rainfall intensity = 4.565(In/Hr)
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	4.760	9.54	4.125
2	2.464	7.93	4.565

Largest stream flow has longer time of concentration
 $Q_p = 4.760 + \text{sum of}$
 $Q_b \quad I_a/I_b$
 $2.464 * 0.904 = 2.227$
 $Q_p = 6.987$

Total of 2 main streams to confluence:
 Flow rates before confluence point:
 4.760 2.464
 Area of streams before confluence:
 1.520 0.610

Results of confluence:
 Total flow rate = 6.987(CFS)
 Time of concentration = 9.536 min.
 Effective stream area after confluence = 2.130(Ac.)
 End of computations, total study area = 2.13 (Ac.)
 The following figures may be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.300
 Area averaged RI index number = 69.8

Item 5.7

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989 - 2005 Version 7.1
Rational Hydrology Study Date: 06/16/15 File:ARTPON100.out

TRACT MAP 36785
POST-PROJECT ON-SITE HYDROLOGY FOR AREA T
100-YEAR STORM EVENT
FILENAME: ARTPON100.RRV

***** Hydrology Study Control Information *****

English (in-lb) Units used in input data file

Program License Serial Number 6269

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.500(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.500(In/Hr)
Slope of intensity duration curve = 0.5500

Process from Point/Station 2001.000 to Point/Station 2002.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 642.000(Ft.)
Top (of initial area) elevation = 1432.500(Ft.)
Bottom (of initial area) elevation = 1425.100(Ft.)
Difference in elevation = 7.400(Ft.)
Slope = 0.01153 s(percent) = 1.15
TC = $k(0.353) * [(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 11.441 min.
Rainfall intensity = 3.732(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.868
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.330
Decimal fraction soil group D = 0.670
RI index for soil(AMC 2) = 73.00
Pervious area fraction = 0.300; Impervious fraction = 0.700
Initial subarea runoff = 5.153(CFS)
Total initial stream area = 1.590(Ac.)
Pervious area fraction = 0.300

Process from Point/Station 2002.000 to Point/Station 2003.000
**** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 1426.100(Ft.)
Downstream point elevation = 1425.100(Ft.)
Channel length thru subarea = 62.000(Ft.)

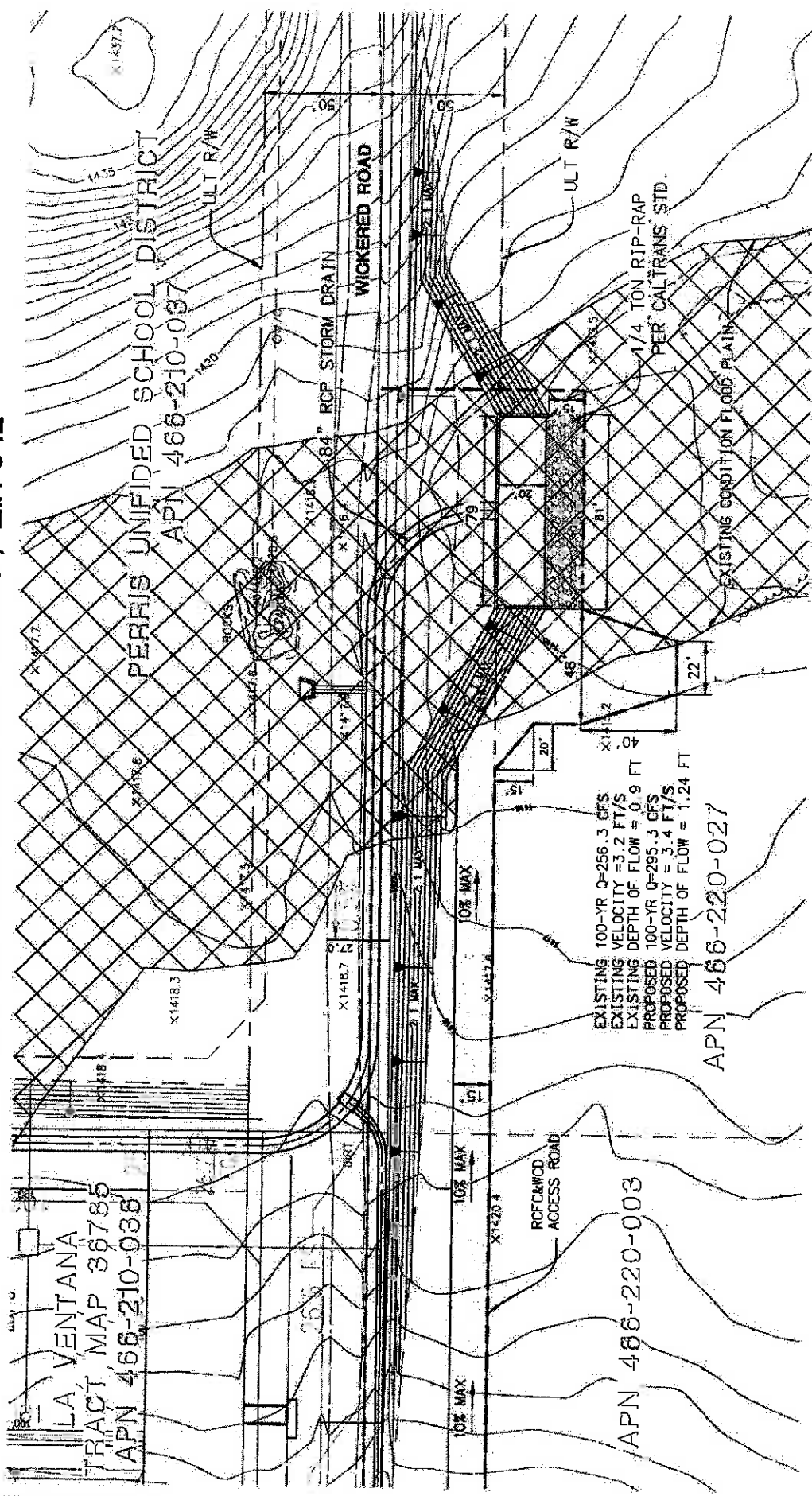
Channel base width = 5.000(Ft.)
Slope or 'Z' of left channel bank = 2.000
Slope or 'Z' of right channel bank = 2.000
Manning's 'N' = 0.025
Maximum depth of channel = 2.000(Ft.)
Flow(q) thru subarea = 5.153(CFS)
Depth of flow = 0.297(Ft.), Average velocity = 3.097(Ft/s)
Channel flow top width = 6.189(Ft.)
Flow Velocity = 3.10(Ft/s)
Travel time = 0.33 min.
Time of concentration = 11.77 min.

Sub-Channel No. 1 Critical depth = 0.309(Ft.)
' ' ' Critical flow top width = 6.234(Ft.)
' ' ' Critical flow velocity = 2.973(Ft/s)
' ' ' Critical flow area = 1.733(Sq.Ft)

Process from Point/Station 2003.000 to Point/Station 2004.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1425.100(Ft.)
Downstream point/station elevation = 1423.100(Ft.)
Pipe length = 240.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 5.153(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 5.153(CFS)
Normal flow depth in pipe = 10.85(In.)
Flow top width inside pipe = 13.42(In.)
Critical Depth = 11.05(In.)
Pipe flow velocity = 5.42(Ft/s)
Travel time through pipe = 0.74 min.
Time of concentration (TC) = 12.51 min.
End of computations, total study area = 1.59 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.300
Area averaged RI index number = 73.0



ALTERNATIVE 1 - LINE 1 STORM DRAIN OUTLET
PROPOSED ACCESS AND EASEMENT



JCS Engineering & Consulting, Inc.
3661 CALLE DE LOBO
MURRIETA, CA 92562
PH. 951.946.5551 FAX 951.946.5568

FIGURE A-1

Larry R. Markham

From: Joe Castaneda
Sent: Wednesday, April 06, 2016 6:13 AM
To: Larry R. Markham
Cc: JRivani@GIDLLCO.COM
Subject: RE: La Ventana- Tract Map 36785
Attachments: LINE 1 OUTLET_ALT #1 and Alt #2.pdf

Larry,

Based on conversation on Friday April 1, 2016 we did the following to provide more information related to the design of the storm drain entering the Neumann property:

1. We evaluated the 100 year flood plain and placed it on the two alternatives that we discussed on Friday. The exhibits show the limits of the 100 year flood plain in blue. In order to make the exhibits less cumbersome I removed the cross sections used to evaluate the flood plain. The flood plain was assessed using HEC-RAS. We placed the existing flow rate and velocity on the exhibit.
2. On alternative 1 and 2 we relocated the limits of the storm drain system and the culvert to extend to the future right-of-way as we discussed on Friday. We also provided the anticipated grading required over the system that is needed to extend the systems to the right-of-way.
3. We assessed the proposed velocity using the post-project condition flow rate that would be discharged by the project. The analyses we did for the project assessed hydromodifications and the RCFC&WCD interim design criteria. As you know, the interim design criteria requires mitigation for the 2, 5, and 10 year storms. We did not assess the 100 year, 1 hour. However, based on the projects we have been working we have noticed that the hydromodification criteria is so onerous that mitigating the 100 year, 1 hour is not difficult to do.
4. The outlet velocities were calculated using a normal depth analysis across the rip-rap dissipator.
5. The following are descriptions of the Alternatives:
 - a. **Alternative #1:** This is a conventional storm drain solution that would require the system to be maintained by RCTD or RCFC. As I mentioned, this is the schools preferred alternative. The storm drain system would be located along the centerline of Wickered Road. We would discharge the flow rate into a stilling basin with a downstream impact wall to reduce the velocities and recreate the sheet flow condition. A 15 feet rip-rap dissipator would be used downstream of the stilling basin. The rip-rap dissipator would implement the use of a concrete grade beam downstream of the rip-rap to ensure flows are distributed in a manner similar to what occurs today.
 - b. **Alternative #2:** This a design in which we discharge flows onto the school site. The flows would go through the school site and flow towards Wickered Road. This solution implements the use of 3-14'W x 7'H RCBs that would allow for the flows to be spread in a sheet flow condition. Wingwalls would be constructed and a rip-rap dissipator would be used to reduce the flow rate exiting the RCB.

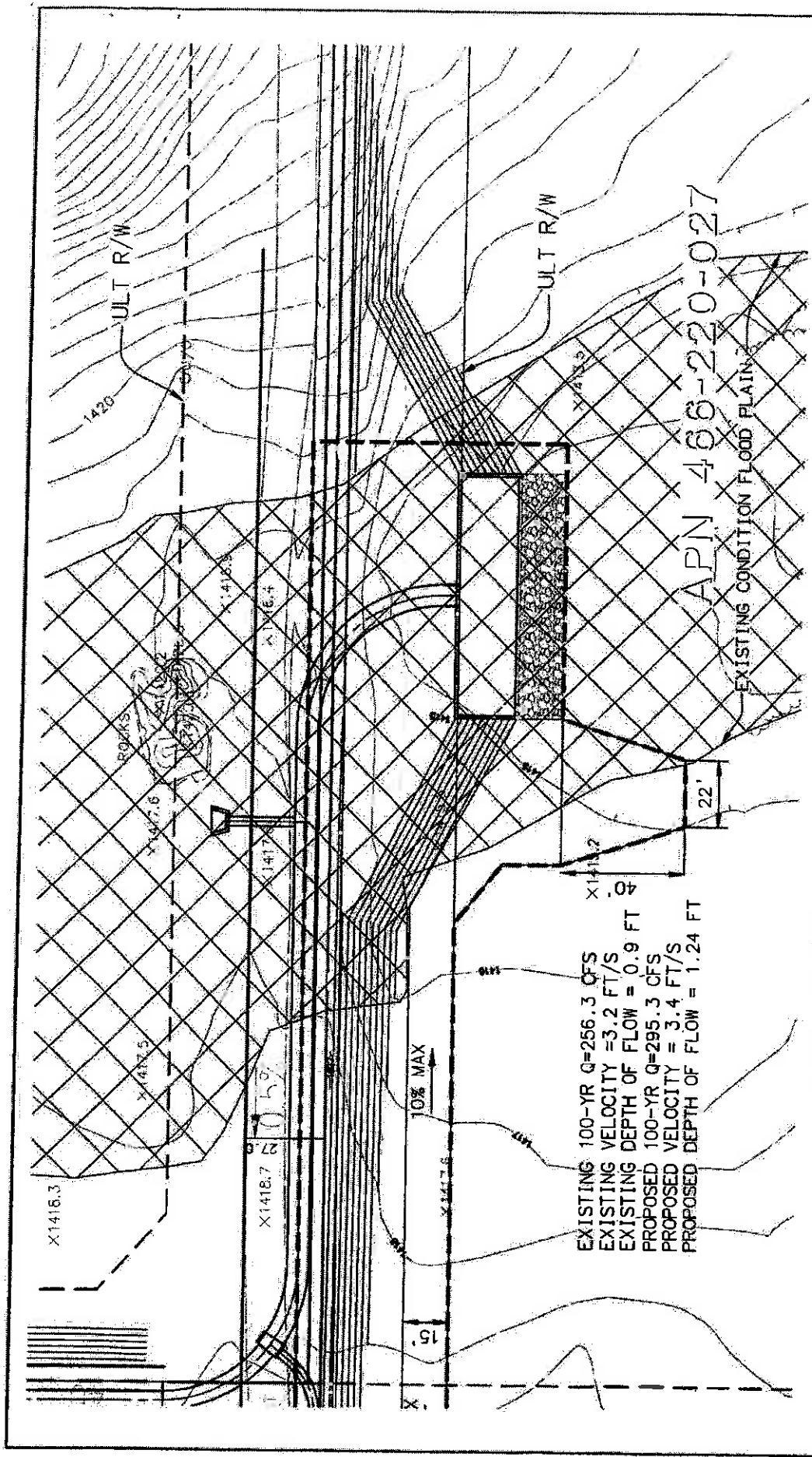
Please review the revisions and do not hesitate to call with any questions.

Joe Castaneda P.E.

President
:: 951.304.9552 – Office
:: 951.304.3568 – Fax

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38263 Calle de Lobo
Murrieta, CA 92562





X1416.3

X1417.5

X1418.7

X1419.9

X1421.1

X1422.3

X1423.5

X1424.7

X1425.9

X1427.1

X1428.3

ULT R/W

ULT R/W

APN 466-220-027

EXISTING CONDITION FLOOD PLAIN

EXISTING 100-YR Q=256.3 CFS
 EXISTING VELOCITY = 3.2 FT/S
 EXISTING DEPTH OF FLOW = 0.9 FT
 PROPOSED 100-YR Q=295.3 CFS
 PROPOSED VELOCITY = 3.4 FT/S
 PROPOSED DEPTH OF FLOW = 1.24 FT

10% MAX

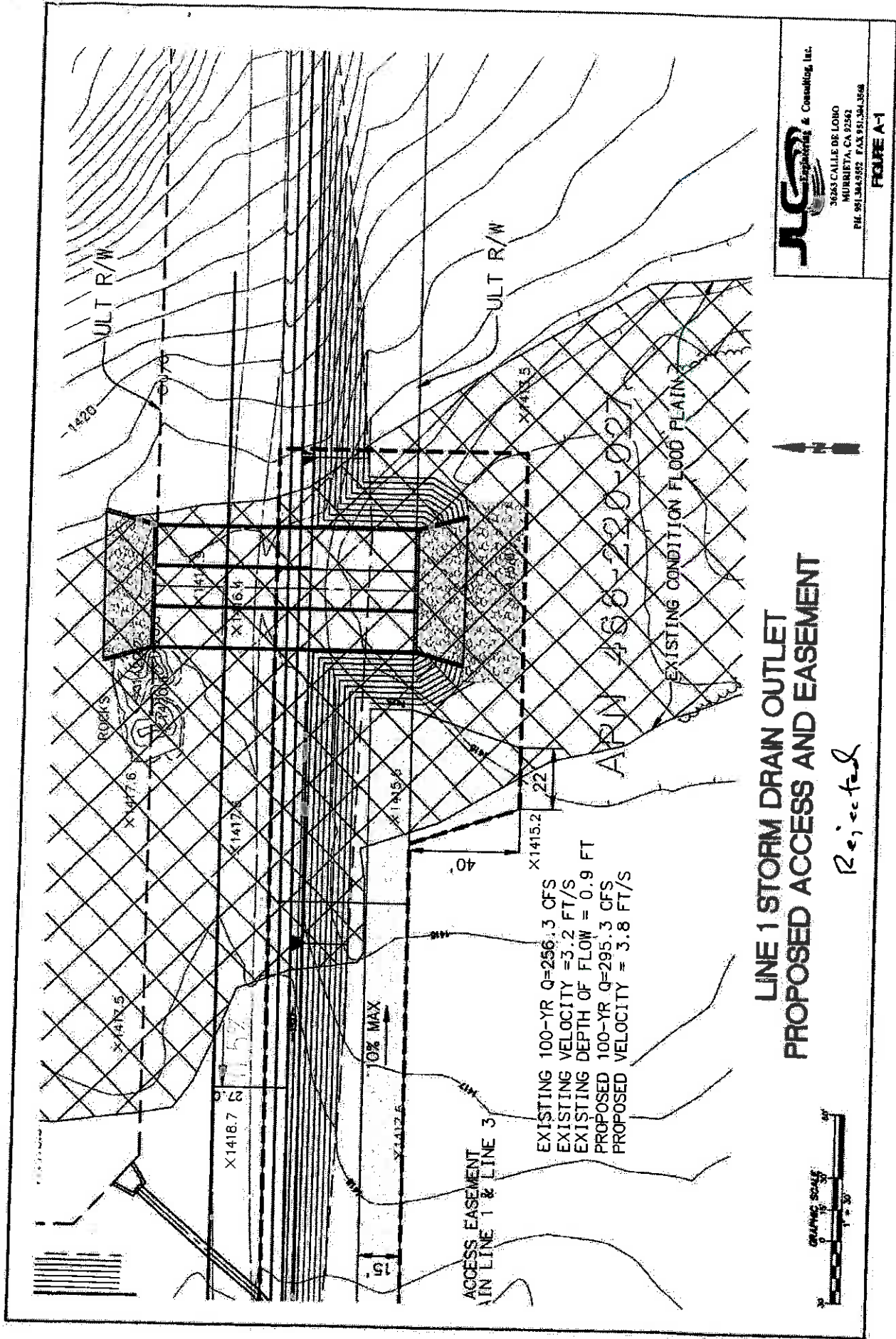
22'

**LINE 1 STORM DRAIN OUTLET
PROPOSED ACCESS AND EASEMENT**



36263 CALLE DE LOBO
 MURRIETA, CA 91542
 PH. 951.94.9552 FAX 951.94.5569

FOUR A-1



ACCESS EASEMENT
IN LINE 1 & LINE 3

EXISTING 100-YR Q=256.3 CFS
 EXISTING VELOCITY = 3.2 FT/S
 EXISTING DEPTH OF FLOW = 0.9 FT
 PROPOSED 100-YR Q=295.3 CFS
 PROPOSED VELOCITY = 3.8 FT/S

**LINE 1 STORM DRAIN OUTLET
 PROPOSED ACCESS AND EASEMENT**

Rejected

JCS
 Engineering & Consulting, Inc.
 3685 CALLE DE LOBO
 MURRIETA, CA 92562
 PH. 925.944.882 FAX 925.944.3508

FIGURE A-1

Clerk's Original



RIVERSIDE COUNTY
PLANNING DEPARTMENT

Steve Weiss AICP
Planning Director

Memorandum

Date: July 12, 2016

To: Board of Supervisors

From: Brett Dawson, Project Planner, Planning Department

RE: Updated Information for Agenda Item 16.1 (General Plan Amendment No. 1129, Change of Zone No. 7856, Tentative Tract Map No. 36785, Environmental Impact Report No. 542.)

To the Honorable Chair,

- Included are additional signatures in support of the project provided by the applicant Mike Naggar.
- Included are two letters from Delano and Delano.
- Attached is a letter from Valley Wide Recreation and Park District.
- Included is a letter to the Board of Supervisors from Andy and Cindy Domenigoni.
- 50.TRANS.023 MAP- OFF SITE IMPROVEMENTS was revised regarding the Line 1 Storm Drain which outlets at the ultimate south Wickerd Road right-of-way line. The end of the condition states, "To implement this condition the adjoining property right of way, and easements as required by RCFC&WCD for the design, construction and maintenance of the Line 1 Storm drain system.

Or as approved by the Director of Transportation." The condition has been revised to remove "Or as approved by the Director of Transportation."

- 90.TRANS.1 MAP – WRCOG TUMF was revised to state "Prior to the issuance of an occupancy permit, the project proponent shall pay the Transportation Uniform Mitigation Fee (TUMF) in accordance with the fee schedule in effect at the time of issuance, pursuant to Ordinance No. 824."
- 80.TRANS.2 MAP – R&BBD was revised to state:
"The project is not required to participate in the Scott Road CFD 05-8.

Prior to the time of issuance of a building permit, the project proponent shall pay fees in accordance with Zone A of the Scott Road and Bridge Benefit District (RBBB) fee schedule in effect at the time of payment. The project proponent may be eligible to pay a reduced Scott Road RBBB fee in accordance with Zone A, in lieu of Zone A1, as indicated in the fee schedule

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P.O. Box 1409, Riverside, California 92502-1409
(951) 955-3200 · Fax (951) 955-1811

Desert Office · 77-588 El Duna Court, Suite H
Palm Desert, California 92211
(760) 863-8277 · Fax (760) 863-7040

07-12-2016
16-1

in effect at the time of these conditions. It should be noted that RBBD fee schedules may be amended in the future, and the fee schedule in effect at the time of payment will govern.

NOTE: The project gross acreage is 170.8 acres and proposed 511 residential lots.

This condition shall not be deferred to occupancy permit.”

- 50.TRANS.10 MAP- DEDICATION Has been revised at the end of the condition, following “A minimum 6’ bike lane shall be striped on the roadway and shall conform to the Caltrans Highway Design Manual.” To state:

“or as approved by the Director of Transportation for any of the conditions described above.

Sufficient public street right-of-way along Meadowgate Lane shall be conveyed for public use to provide for a 30 foot half-width right-of-way. Areas designated as culturally sensitive shall be omitted for the area to be dedicated. Any projects that would improve Meadowgate Lane shall consult with the Pechanga Band of Lusieno Indians or other Native American Indian Tribes.” And “or as approved by the Director of Transportation” has been removed.

In addition to the findings and conclusions in the attached staff report and Environmental Impact Report No. 542, Planning staff would like to provide additional facts supporting the approval recommendation for Tentative Tract Map No. 36785. Tentative Tract Map No. 36785 is not located within a boundary of an existing Specific Plan. Tentative Tract Map No. 36785 is associated with General Plan Amendment No. 1129 which will change the property’s Foundation Component to Community Development and its land use designation to Medium Density Residential. The medium density residential land use designation provides for single family homes and suburban subdivisions with a density range between 2 to 5 dwelling units. Lot sizes within this land use designation range from 5,500 to 20,000 square feet. Tentative Tract Map No. 36785 proposes a subdivision for single family homes with a density of approximately 2.9 dwelling units per acre and a minimum lot size of 5,500. Additionally, General Plan Amendment No. 1129 proposed to remove the project site from the Rural Residential Area East of Interstate 215 Policy Area. Once removed, there will be no further conflict or internal inconsistency regarding residential development densities. Therefore, Tentative Tract Map No. 36785 is consistent with the property’s General Plan land use designation as amended by proposed General Plan Amendment No. 1129.

Furthermore, the design of the proposed Tentative Tract Map No. 36785 is consistent with the County’s General Plan. The General Plan’s Vision Statement encourages critical community facilities such as parks, schools, healthcare and mental health facilities to be distributed throughout Riverside County so that they are accessible to and benefit all residents. The Vision Statement also emphasizes the importance of partnerships between school districts and local governments in providing quality educational facilities in the County. Appendix B of the General Plan, Principle II.C. and IV.G., encourages usable open space, parks connected to schools and recreational facilities that are available for persons of all ages to enjoy. Tentative Tract Map No. 36785 includes a park and open space along the eastern edge of the site, bordering the new high school. This park will include ball fields including baseball and soccer fields. These can be used for joint use, allowing the school to have more activities. Additionally, the proposed project will include a park specially designed for person with disabilities. The project’s design will act as a buffer between the school use and the remaining rural community and provide a transition from the proposed medium density subdivision to the existing rural community.

Additionally, Principle IV.A.1 provides that the intent of the General Plan is to foster variety and choice in community development, particularly in the choice and opportunity for housing in various styles, of varying densities and of a wide range of prices and accommodating a range of life styles in equally diverse community settings, emphasizing compact and higher density choices. Moreover, Principle IV.A. 4 provides that low density residential development should not be the predominant use or standard by which residential desirability is determined. Tentative Tract Map No. 36785 will create a transition of housing density ranges from Medium Density Residential along Scott Road to larger lot requirements to the north, which is consistent with the principle to provide a variety of housing products and lot sizes.

The site is physically suitable for the proposed residential development and density because it consists of lightly rolling terrain, is not located within either a CAL Fire state responsibility area or a very high fire hazard severity zone and is not located within a Criteria Area of the Multi-Species Habitat Conservation Plan. Additionally, higher density development is consistent with the recent approvals of General Plan Amendment Nos. 921 and 928 and project's conditions of approval will also improve access for the site and surrounding area. The parks and athletic fields included in Tentative Tract Map No. 36785 will also serve as recreational areas for the development's residents.

Environmental Impact Report No. 542 (EIR No. 542) was prepared for the project which includes General Plan Amendment No. 1129, Change of Zone No. 7856 and Tentative Tract Map No. 36785. EIR No. 542 analyzed the project's potential significant effects on the environment and made the required findings in compliance with the State CEQA Guidelines and Riverside County CEQA implementing projects. Based on the findings and conclusions in EIR No. 542 and the project's conditions of approval, the design of Tentative Tract Map No. 36785 is not likely to cause serious public health problems.

The design of Tentative Tract Map No. 36785 will not conflict with easements, acquired by the public at large, for access through or use of, property within the proposed subdivision. Within the tentative map there are existing recorded easements for public access roads, however, through the project's design these easements for public access will be maintained or alternatives will be provided. Additionally, in accordance with Section 3.2.J. of Ordinance No. 460, the applicant has provided written assurances (copies of which are attached) from the owners of the properties underlying the off-site improvement/alignment (as shown on the Tentative Map) that sufficient right-of-way can and will be provided.

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CALL (951) 368-9710
EMAIL billinginquiry@pe.com

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Placed by: Cecilia Gil

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I am a citizen of the United States. I am over the age of eighteen years and not a party to or interested in the above entitled matter. I am an authorized representative of THE PRESS-ENTERPRISE, a newspaper in general circulation, printed and published daily in the County of Riverside, and which newspaper has been adjudicated a newspaper of general circulation by the Superior Court of the County of Riverside, State of California, under date of April 25, 1952, Case Number 54446, under date of March 29, 1957, Case Number 65673, under date of August 25, 1995, Case Number 267864, and under date of September 16, 2013, Case Number RIC 1309013; that the notice, of which the annexed is a printed copy, has been published in said newspaper in accordance with the instructions of the person(s) requesting publication, and not in any supplement thereof on the following dates, to wit:

07/02/2016

I certify (or declare) under penalty of perjury that the foregoing is true and correct.

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At: Riverside, California


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NOTICE OF PUBLIC HEARING BEFORE THE BOARD OF SUPERVISORS OF RIVERSIDE COUNTY ON A GENERAL PLAN AMENDMENT, CHANGE OF ZONE, AND A TENTATIVE TRACT MAP IN THE THIRD SUPERVISORIAL DISTRICT AND NOTICE OF INTENT TO CERTIFY AN ENVIRONMENTAL IMPACT REPORT

NOTICE IS HEREBY GIVEN that a public hearing at which all interested persons will be heard, will be held before the Board of Supervisors of Riverside County, California, on the 1st Floor Board Chambers, County Administrative Center, 4080 Lemon Street, Riverside, on **Tuesday, July 12, 2016 at 10:30 A.M.** or as soon as possible thereafter, to consider the application submitted by Joseph Rivani - Jeff Anderson on **General Plan Amendment No. 1129**, which proposes an Extraordinary Foundation Level Amendment to amend the land use from Rural Community: Estate Density Residential (RC:EDR) (2-Acre Minimum) to Community Development: Medium Density Residential (CD:MDR) (2-5 dwelling units per acre) and Open Space: Recreation (OS:R), to modify the General Plan to remove the Estate Density and Rural Residential East of Interstate 215 Policy Area from the project site, and to amend the Circulation Element to downgrade La Ventana road within the project boundary (between Garbani Road and Wickerd Road) from a Secondary Highway to a Collector; **Change of Zone No. 7856**, which proposes to change the zone from Residential Agricultural 5-Acre Minimum (R-A-5) to Planned Residential (R-4), or such other zones as the Board may find appropriate; **Tentative Tract Map No. 36785, Schedule A**, which proposes to subdivide 170.8 gross acres into 511 residential lots with a 5,500 sq. ft. minimum lot size, and 25 lettered lots consisting of drainage basins, parks, paseos, and open space. The project is located northerly of Wickerd Road, easterly of Heinz Lane, southerly of Garbani Road, and westerly of Brandon Lane in the Winchester Zoning - Sun City / Menifee Valley Area Plan, Third Supervisorial District.

The Planning Commission approved the project, found that the environmental effects have been addressed and recommended the certification of **Environmental Impact Report No. 542**.

The project case file may be viewed from the date of this notice until the public hearing, Monday through Friday, from 8:00 a.m. to 5:00 p.m. at the Clerk of the Board of Supervisors at 4080 Lemon Street, 1st Floor, Riverside, California 92501, and at the Riverside County Planning Department at 4080 Lemon Street, 12th Floor, Riverside, California 92501.

FOR FURTHER INFORMATION REGARDING THIS PROJECT, PLEASE CONTACT BRETT DAWSON, PROJECT PLANNER, AT (951) 955-0972 OR EMAIL BDawson@rcplma.org.

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Alternative formats available upon request to individuals with disabilities. If you require reasonable accommodation, please contact Lisa Wagner at (951) 955-1063, 72 hours prior to the hearing.

Please send all written correspondence to: Clerk of the Board, 4080 Lemon Street, 1st Floor, Post Office Box 1147, Riverside, CA 92502-1147

Dated: June 29, 2016
Kecla Harper-Ihem, Clerk of the Board
By: Cecilia Gil, Board Assistant

7/2

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Dated: June 29, 2016

Kecia Harper-Ihem, Clerk of the Board
By: Cecilia Gil, Board Assistant

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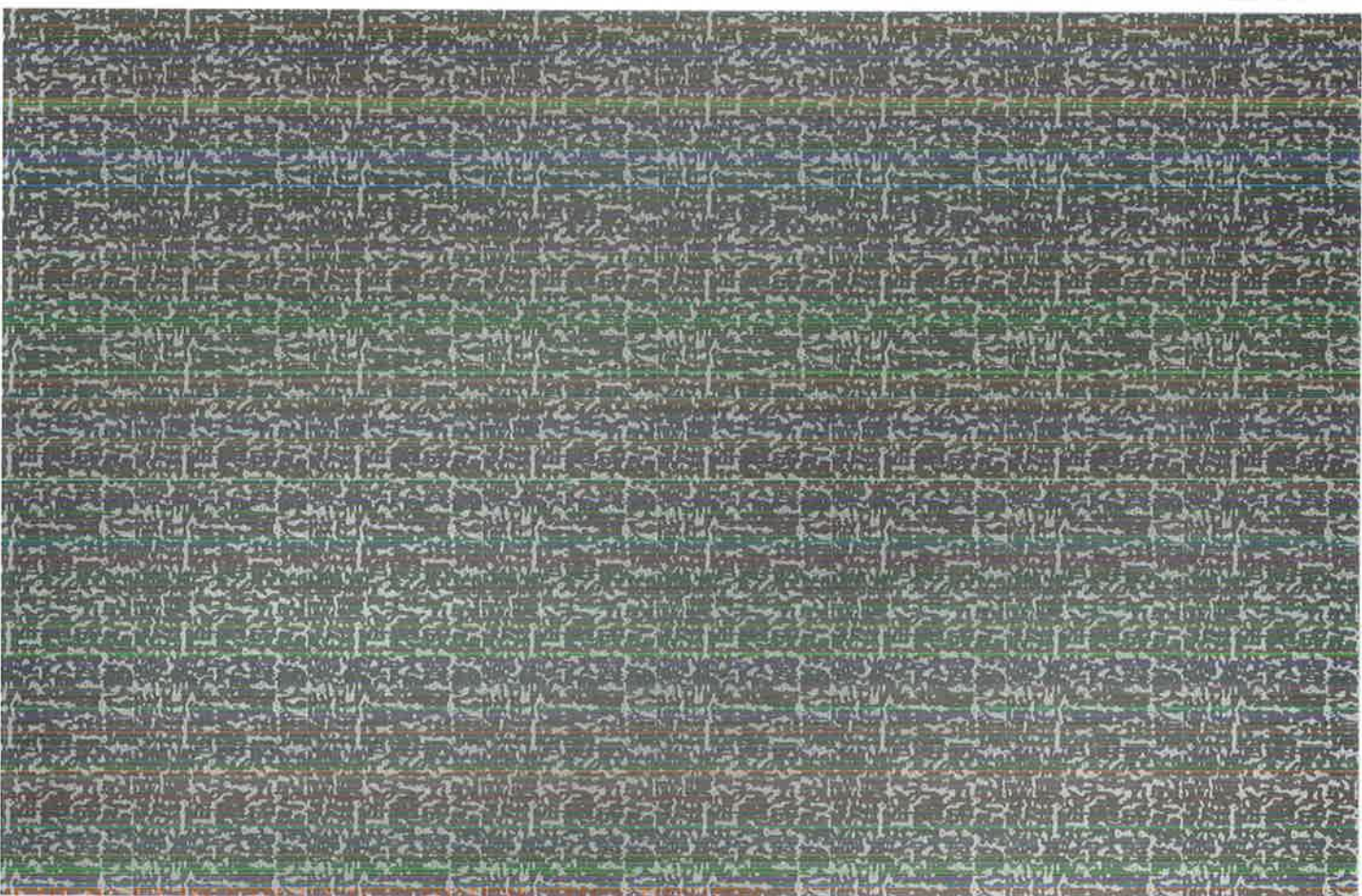
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NOTICE OF PUBLIC HEARING BEFORE THE BOARD OF SUPERVISORS OF RIVERSIDE COUNTY ON A GENERAL PLAN AMENDMENT, CHANGE OF ZONE, AND A TENTATIVE TRACT MAP IN THE THIRD SUPERVISORIAL DISTRICT AND NOTICE OF INTENT TO CERTIFY AN ENVIRONMENTAL IMPACT REPORT

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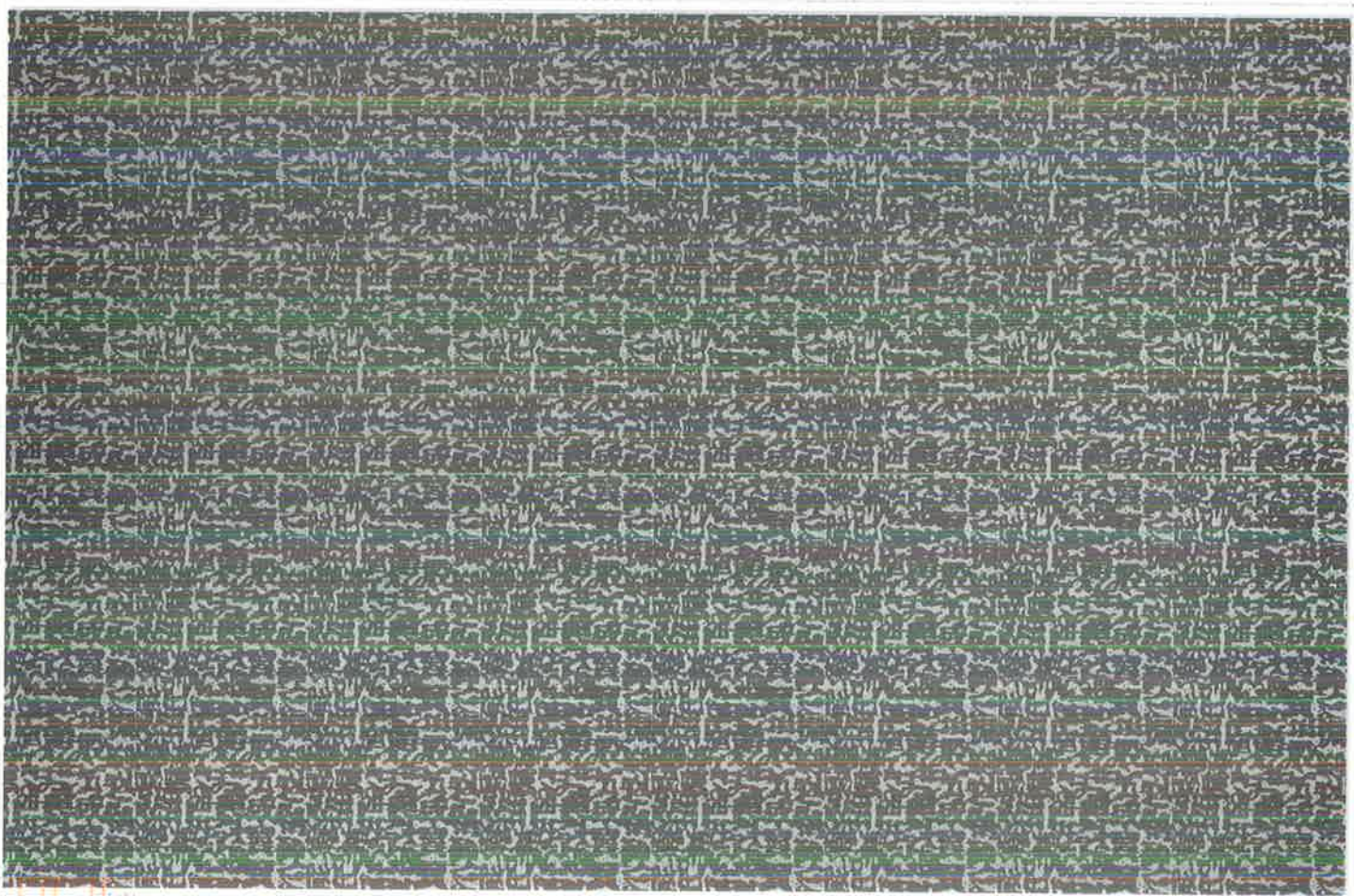
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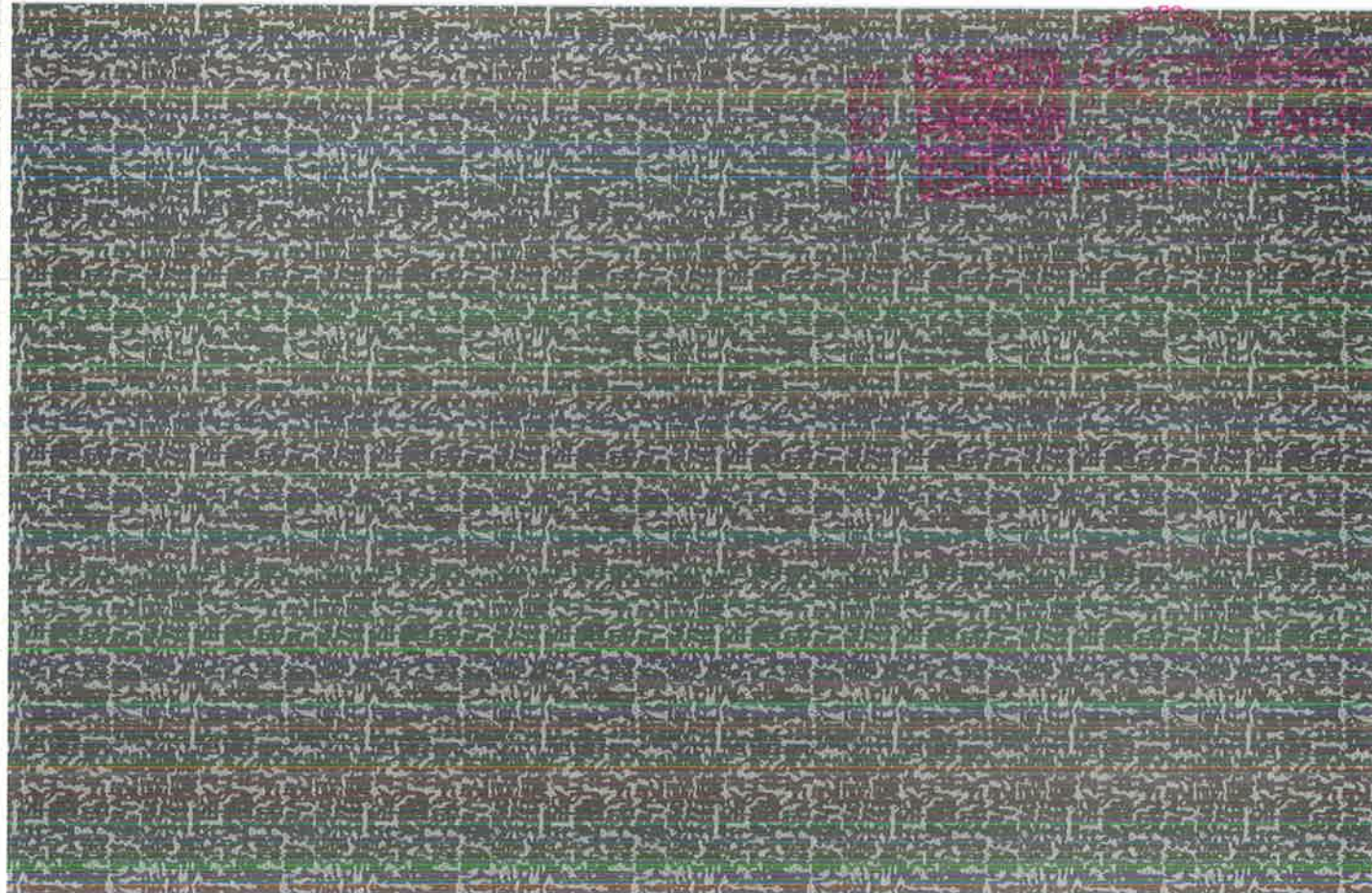
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Please send all written correspondence to: Clerk of the Board, 4080 Lemon Street, 1st Floor, Post Office Box 1147, Riverside, CA 92502-1147

Dated: June 29, 2016

Kecia Harper-Ihem, Clerk of the Board
By: Cecilia Gil, Board Assistant

16-1 of 07/12/16



Riverside County Clerk of the Board
County Administrative Center
4080 Lemon Street, 1st Floor Annex
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Planning Commission Riverside County
c/o Mary Stark, Planning Commission
Secretary
Mail Stop 1070

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NOTICE OF PUBLIC HEARING BEFORE THE BOARD OF SUPERVISORS OF RIVERSIDE COUNTY ON A GENERAL PLAN AMENDMENT, CHANGE OF ZONE, AND A TENTATIVE TRACT MAP IN THE THIRD SUPERVISORIAL DISTRICT AND NOTICE OF INTENT TO CERTIFY AN ENVIRONMENTAL IMPACT REPORT

NOTICE IS HEREBY GIVEN that a public hearing at which all interested persons will be heard, will be held before the Board of Supervisors of Riverside County, California, on the 1st Floor Board Chambers, County Administrative Center, 4080 Lemon Street, Riverside, on **Tuesday, July 12, 2016 at 10:30 A.M.** or as soon as possible thereafter, to consider the application submitted by Joseph Rivani – Jeff Anderson on **General Plan Amendment No. 1129**, which proposes an Extraordinary Foundation Level Amendment to amend the land use from Rural Community: Estate Density Residential (RC:EDR) (2-Acre Minimum) to Community Development: Medium Density Residential (CD:MDR) (2-5 dwelling units per acre) and Open Space: Recreation (OS:R), to modify the General Plan to remove the Estate Density and Rural Residential East of Interstate 215 Policy Area from the project site, and to amend the Circulation Element to downgrade La Ventana road within the project boundary (between Garbani Road and Wickerd Road) from a Secondary Highway to a Collector; **Change of Zone No. 7856**, which proposes to change the zone from Residential Agricultural 5-Acre Minimum (R-A-5) to Planned Residential (R-4), or such other zones as the Board may find appropriate; **Tentative Tract Map No. 36785, Schedule A**, which proposes to subdivide 170.8 gross acres into 511 residential lots with a 5,500 sq. ft. minimum lot size, and 25 lettered lots consisting of drainage basins, parks, paseos, and open space. The project is located northerly of Wickerd Road, easterly of Heinz Lane, southerly of Garbani Road, and westerly of Brandon Lane in the Winchester Zoning – Sun City / Menifee Valley Area Plan, Third Supervisorial District.

The Planning Commission approved the project, found that the environmental effects have been addressed and recommended the certification of **Environmental Impact Report No. 542**.

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Dated: June 29, 2016

Kecia Harper-Ihem, Clerk of the Board
By: Cecilia Gil, Board Assistant

16-1 of 07/12/16

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2016 JUL -6 AM 10:55

3rd Supervisor District
Chuck Washington, Supervisor
Board of Supervisors
Riverside County
Mail Stop 1003

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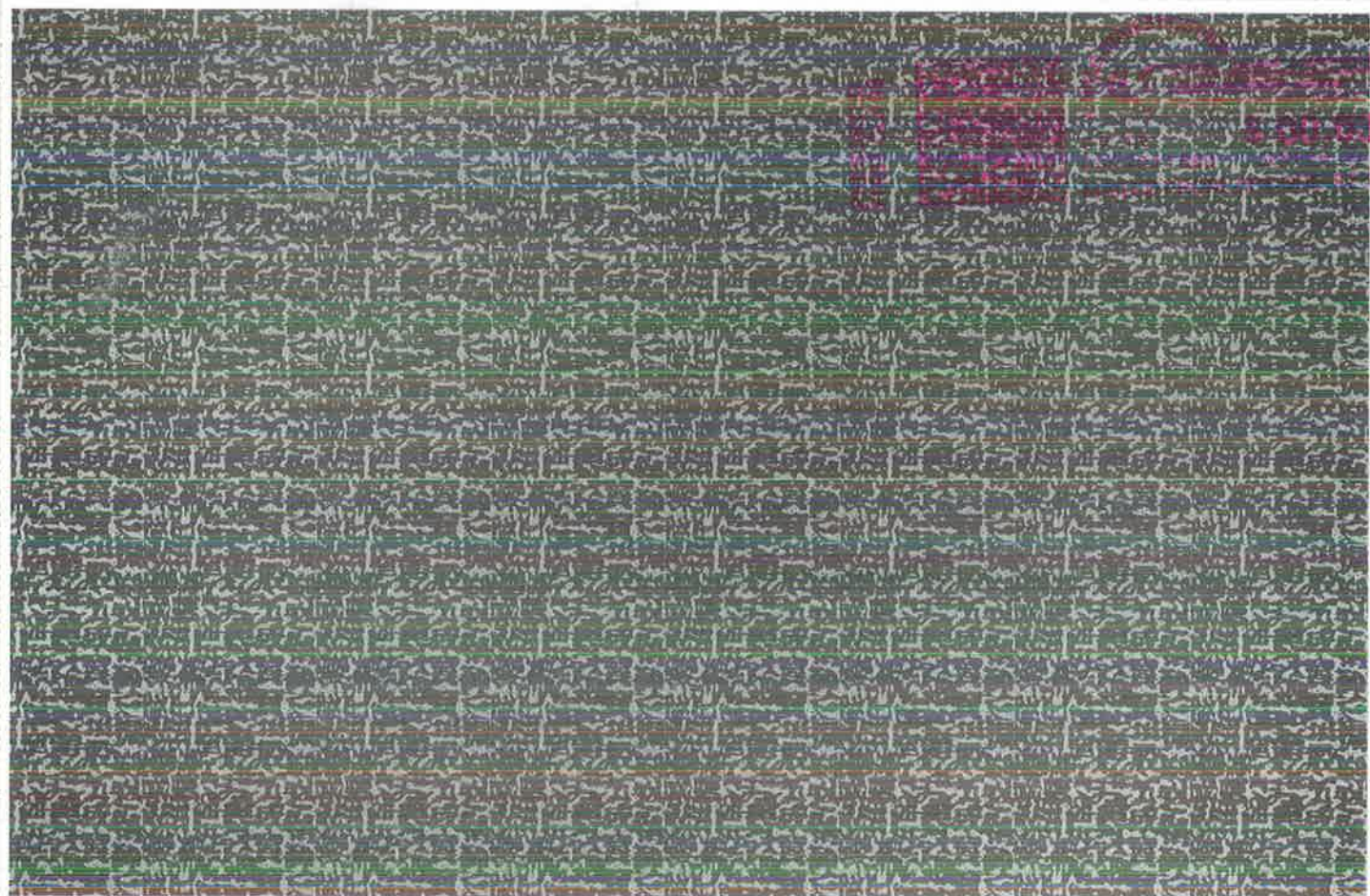
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Riverside, CA 92502-1147



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NOTICE OF PUBLIC HEARING BEFORE THE BOARD OF SUPERVISORS OF RIVERSIDE COUNTY ON A GENERAL PLAN AMENDMENT, CHANGE OF ZONE, AND A TENTATIVE TRACT MAP IN THE THIRD SUPERVISORIAL DISTRICT AND NOTICE OF INTENT TO CERTIFY AN ENVIRONMENTAL IMPACT REPORT

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The Planning Commission approved the project, found that the environmental effects have been addressed and recommended the certification of **Environmental Impact Report No. 542**.

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Dated: June 29, 2016

Kecia Harper-Ihem, Clerk of the Board
By: Cecilia Gil, Board Assistant

16-1 of 07/12/16

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*lot @ this
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UEBERSETZIG LARRY J
31568 RAILROAD CYN RD 130
CANYON LAKE CA 92587

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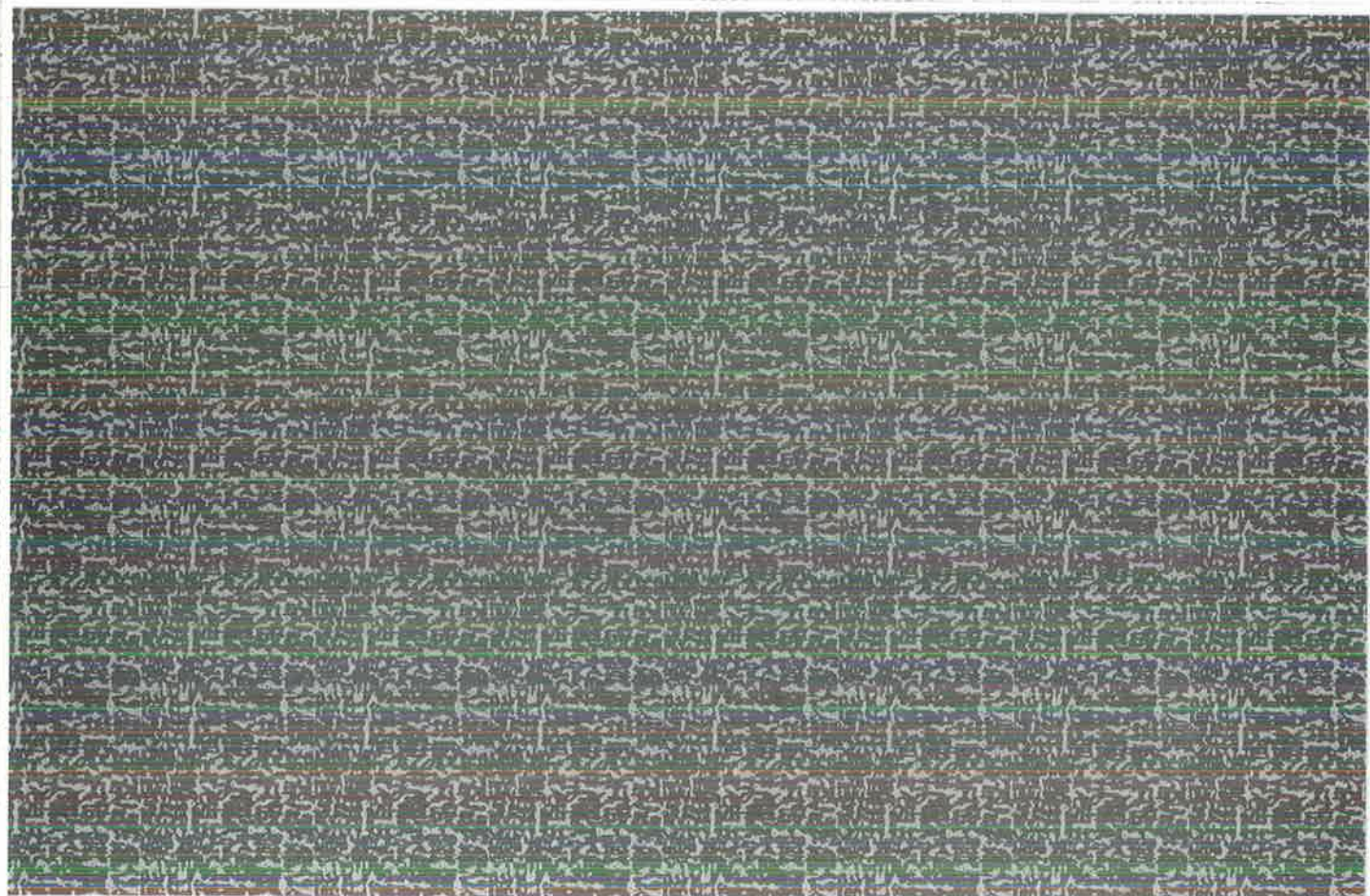


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NOTICE OF PUBLIC HEARING BEFORE THE BOARD OF SUPERVISORS OF RIVERSIDE COUNTY ON A GENERAL PLAN AMENDMENT, CHANGE OF ZONE, AND A TENTATIVE TRACT MAP IN THE THIRD SUPERVISORIAL DISTRICT AND NOTICE OF INTENT TO CERTIFY AN ENVIRONMENTAL IMPACT REPORT

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Dated: June 29, 2016

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By: Cecilia Gil, Board Assistant

16-1 of 07/12/16

BCI: 92502114747 # 0952-03181-05-38
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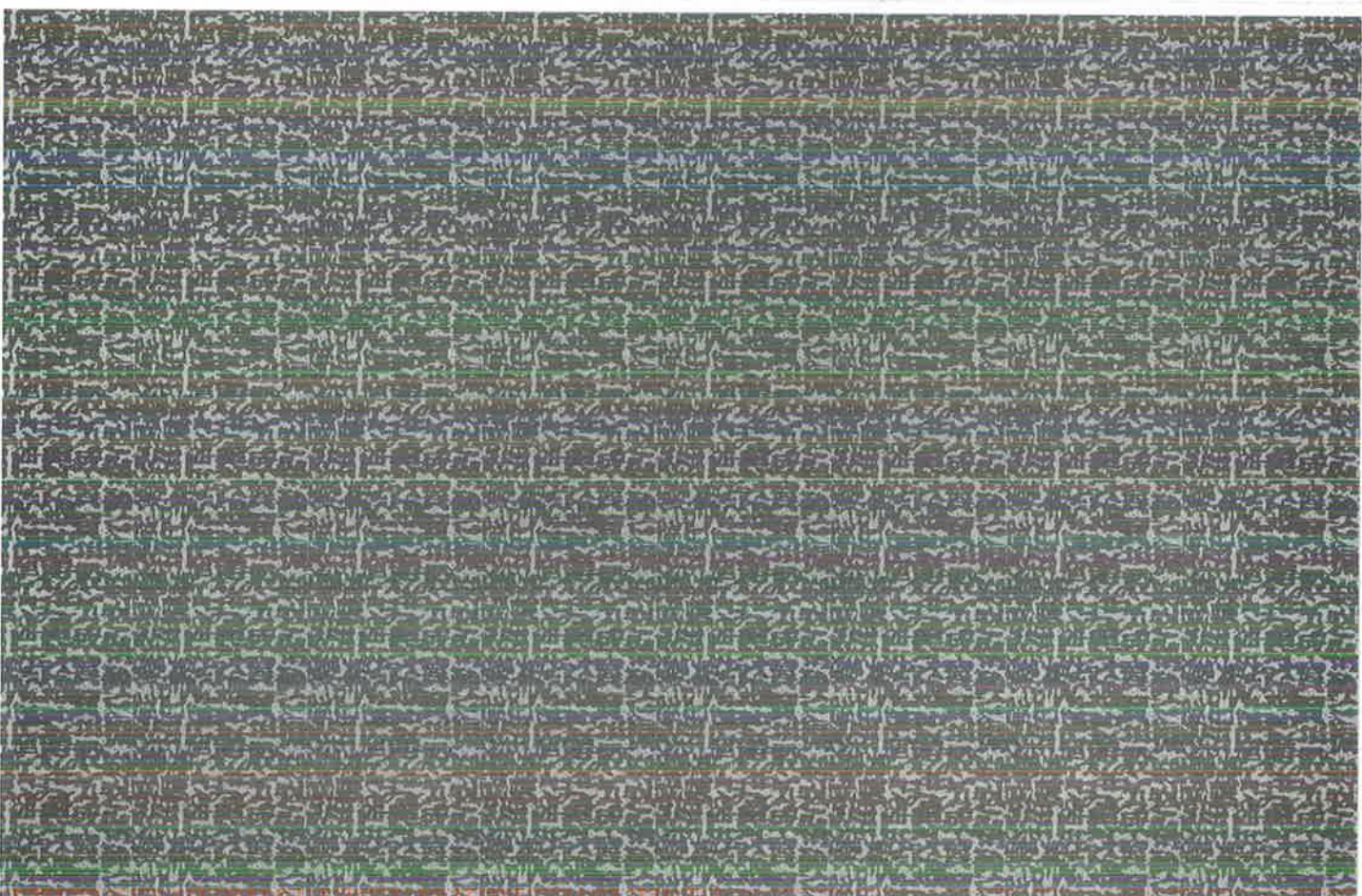
JEFFREY & TERRY MASSIE
29735 KEMPE CIRCLE
MENIFEE CA 92584

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Dated: June 29, 2016

Kecia Harper-Ihem, Clerk of the Board
By: Cecilia Gil, Board Assistant

16-1 of 07/12/16

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UEBERSETZIG LARRY J
31568 RAILROAD CYN RD 130
CANYON LAKE CA 92587

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Riverside, CA 92502-1147

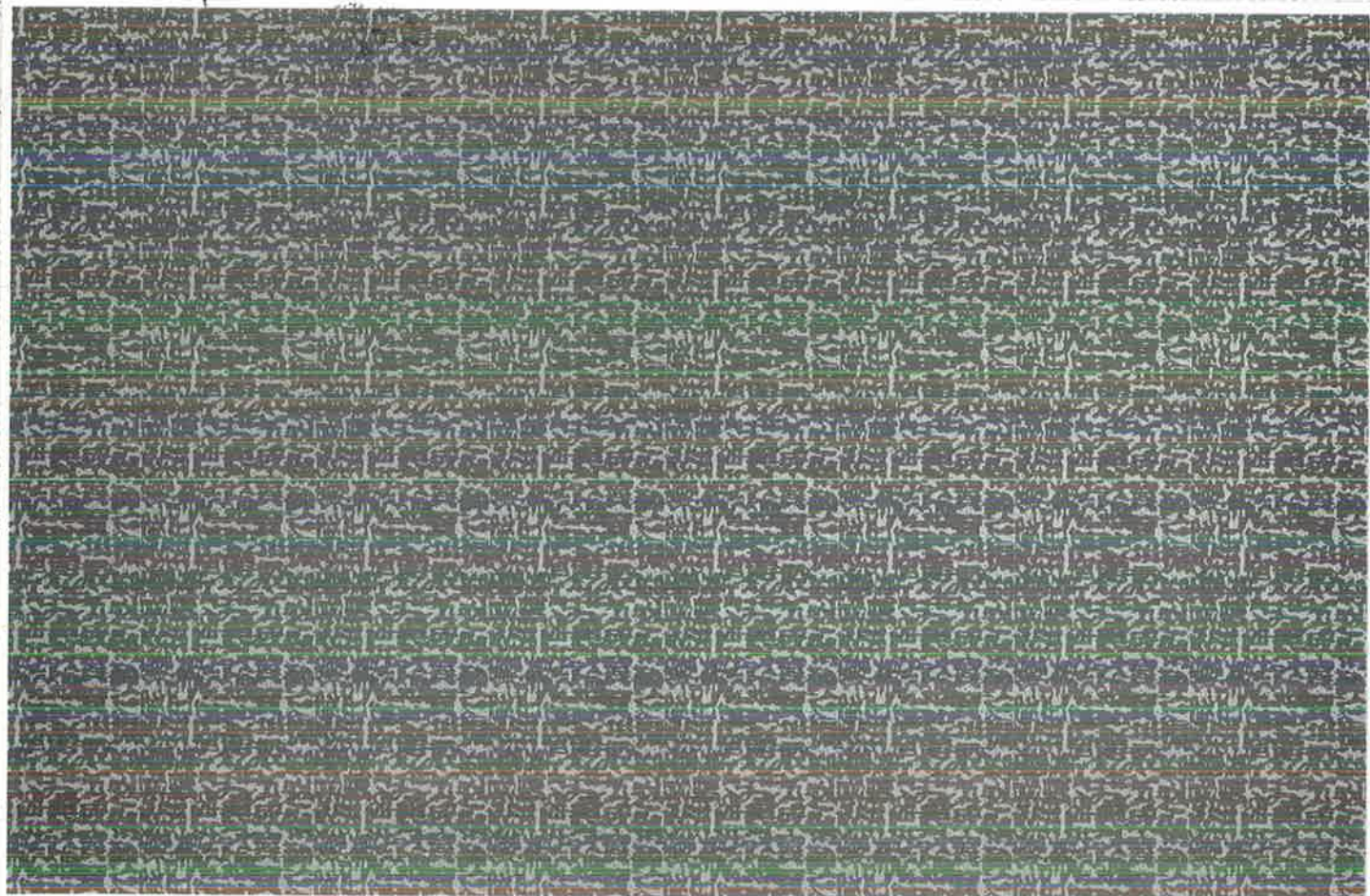
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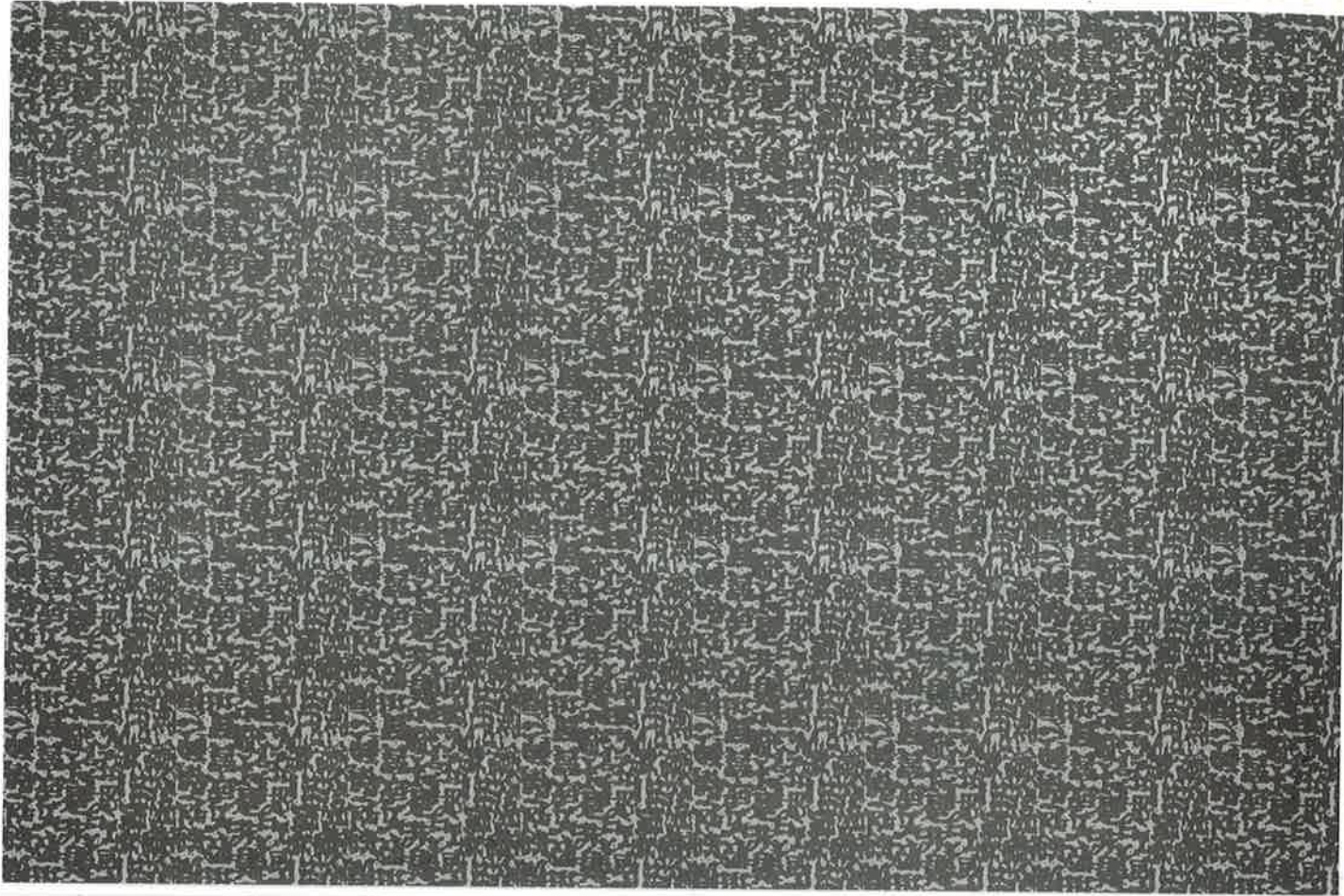
Dated: June 29, 2016

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16-1 of 07/12/16



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Riverside County Clerk of the Board
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2016 JUL 18 PM 1:04

REGIONAL WATER QUALITY CONTROL
BOARD - SAN DIEGO REGION (9)
ENVIRONMENTAL REVIEW
9174 SKY PARK COURT, SUITE 100
SAN DIEGO CA 92123-4340

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Sender*

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